

# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

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**.01.00.00 CATALYST MONITORING**

There are two diagnostic functions, which are used for monitoring of the catalyst efficiency. Both are based on measure of the Oxygen within the catalyst determined by at least two Oxygen sensors. Each of the functions can be correlated between Oxygen / Hydrocarbon and Oxygen/ Oxides of Nitrogen.

**.01.01.00.....Passive measurement of amplitude ratio**

**.01.01.01 General description**

The method compares the signal amplitudes obtained from the downstream sensor to the modelled signal amplitudes. The modelled signal amplitudes are derived from a borderline catalyst. The data for borderline catalysts are taken from measurement results on real life deteriorated catalysts. In case the measured amplitudes exceed those of the model, the catalyst is considered defective. This information is evaluated within one single engine load and speed range (detection over full range of engine load versus speed).

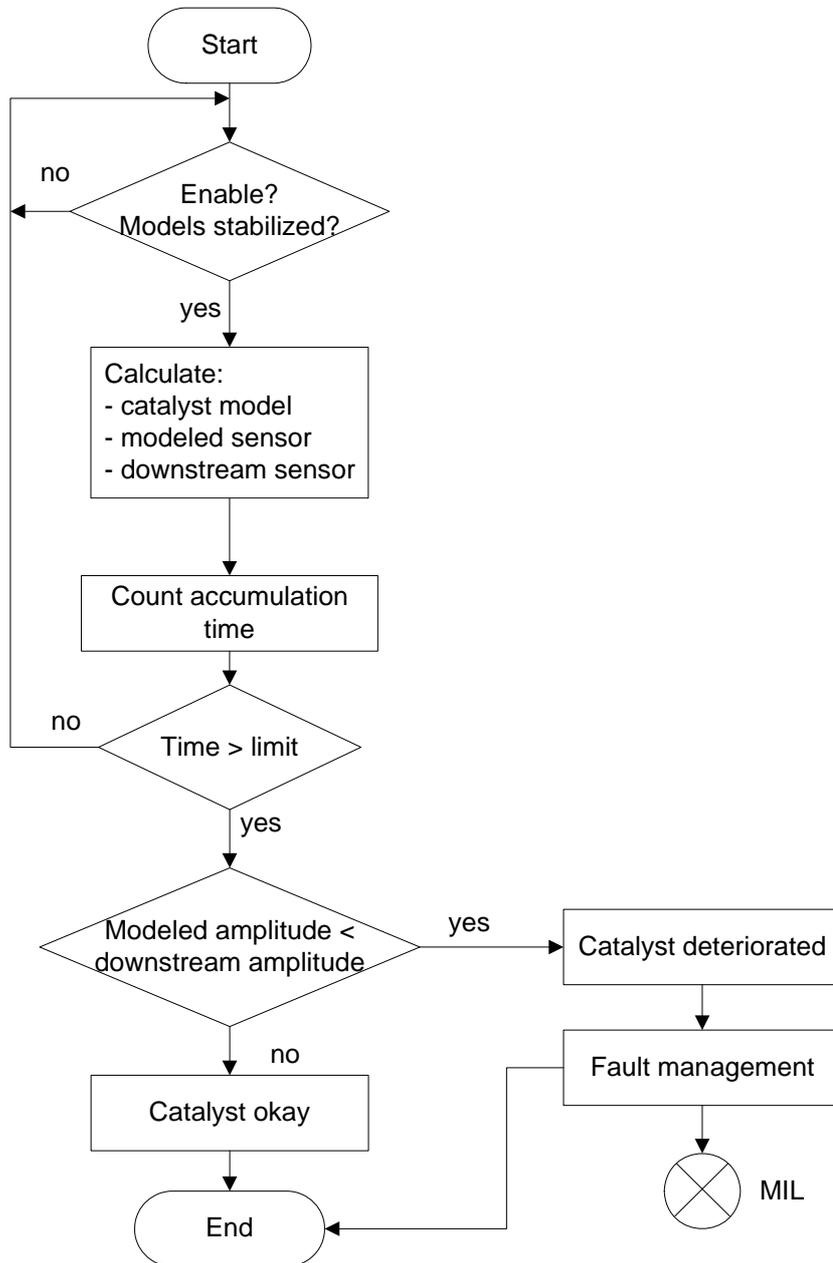
According to the described operating principle the following main parts can be distinguished:

- **Computation of the amplitude of the downstream oxygen sensor:**  
The amplitude of the signal oscillations of oxygen sensor downstream catalyst is calculated. Extracting the oscillating signal component, computing the absolute value and averaging over time accomplish this.
- **Modelling of a borderline catalyst and of the signal amplitudes of the downstream oxygen sensor:**  
The model is simulating the oxygen storage capability of a borderline catalyst. The signal of the downstream oxygen sensor is simulated in the catalyst model based on real time engine operating data (e.g. A/F ratio and engine load). The amplitude of the modelled signal oscillations is calculated.
- **Signal and fault evaluation**  
The signal amplitudes of the downstream oxygen sensor are compared with the model for a given time. In case of the signal amplitudes of the downstream sensor exceed the modelled amplitudes, the oxygen storage capability of the catalyst falls short of the borderline catalyst model.
- **Check of monitoring conditions**  
It is necessary to check the driving conditions for exceptions where no regular Lambda control is possible, e.g. fuel cut-off. During these exceptions, and for a certain time afterwards, the computation of the amplitude values and the post processing is halted. Thus, a distortion of the monitoring information is avoided.

**.01.01.02 Monitoring Structure**

The catalyst temperature (model) activates the catalyst monitoring function if the catalyst temperature is above a predetermined value.

**.01.01.03 Flow Chart Catalyst Monitoring**



**.01.02.00 ..... Active measurement of OSC**

**.01.02.01      General description**

The catalyst monitor is based on the determination of oxygen storage capability (OSC). The correlation between conversion efficiency and the OSC has been investigated on catalysts with various characteristics specifically concerning stages of aging correlated to exhaust emissions (HC/NOx). Therefore, the catalyst is diagnosed by comparing its storage capability against the storage capability of a borderline catalyst.

The oxygen storage capability (OSC) can be determined by one of the following two methods:

**1. Oxygen reduction after fuel-cut (Quick pass of the monitor)**

Oxygen is stored in the catalyst during fuel-cut conditions happening while driving the vehicle. After fuel-cut, the catalyst is operated with a rich air-fuel ratio (A/F) and the amount of removed oxygen is determined. If this passive test indicates an OSC value highly above the borderline catalyst, the catalyst is diagnosed without an error. This monitoring path can only generate a "pass" result.

**2. Determination of Oxygen storage (active test)**

For purposes of monitoring, the ECM cycles the A/F ratio by commanding a rich and a lean fuel mixture as follows.

- First, ECM commands a rich A/F ratio until a minimum of oxygen has been removed (cumulated rich gas > threshold).
- Then, the catalyst is operated with a lean A/F ratio commanded by ECM and the Oxygen Storage Capability is calculated from the oxygen mass stored in the catalyst as follows:

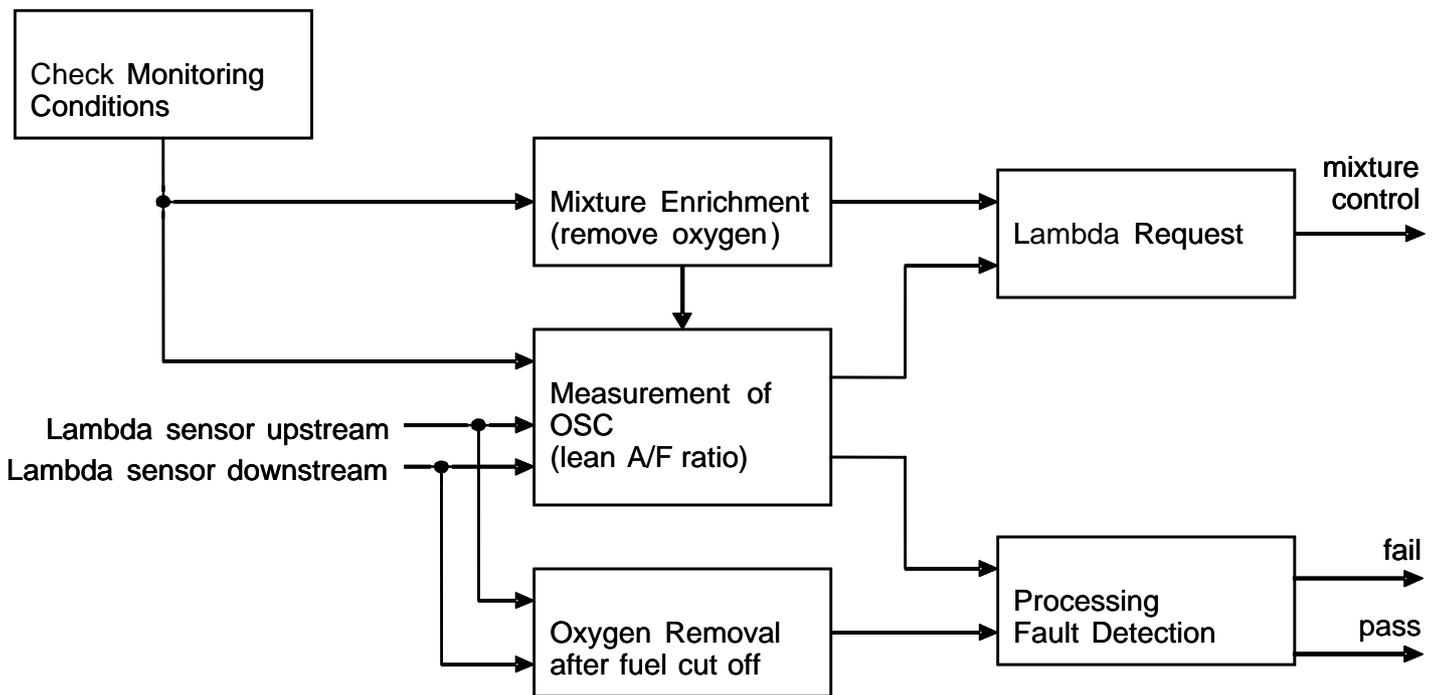
$$\text{OSC} = \int \text{air mass flow} * \text{lean mixture} (\lambda - 1) * dt$$

- The catalyst is operated in this mode until the oxygen stored in the catalyst exceeds a calibrated limit or the downstream oxygen sensor indicates that the catalyst is completely saturated with oxygen.
- The catalyst is then diagnosed by comparing its oxygen storage capability to the calibrated threshold of a borderline catalyst.

## .01.02.02 Monitoring Structure

According to the operating principle described above the following main parts of the monitor can be distinguished:

- Monitoring the amount of removed oxygen after fuel cut off
- Check of monitoring conditions for active test
- Lambda request (interface to lambda controller)
- Mixture enrichment in order to remove any stored oxygen
- Measurement of oxygen storage capacity (OSC) by lean A/F ratio operation
- Processing
- Fault detection



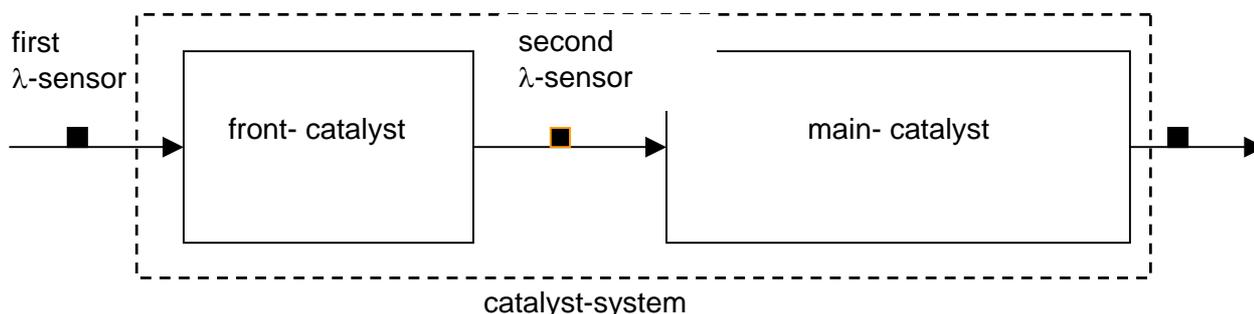
Processing:

After the measurement of the OSC, the OSC-value is normalized to the OSC-value of the borderline catalyst, which is taken from a map, depending on exhaust gas mass flow and catalyst temperature.

The final diagnostic result is calculated by averaging several, normalized OSC-values and compared to the threshold. The measurement of OSC can be carried out consecutive or stepwise.

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For a catalyst system with 3 Oxygen-Sensors this measuring procedure can be applied to different portions. The different alternatives are shown in the table below.



**Table 1:** Necessary conditions to check the different catalyst volume

Secondary parameters	Front-catalyst	Main-catalyst	Catalyst-system
<ul style="list-style-type: none"> <li>• First <math>\lambda</math>-sensor is active</li> <li>• Second <math>\lambda</math>-sensor is active</li> <li>• Modelled exhaust gas temp. in range</li> </ul>	Quick pass		
<ul style="list-style-type: none"> <li>• First <math>\lambda</math>-sensor is active</li> <li>• Second <math>\lambda</math>-sensor is active</li> <li>• Third <math>\lambda</math>-sensor is active</li> <li>• Modelled exhaust gas temp. In range</li> </ul>		Quick pass	
<ul style="list-style-type: none"> <li>• First <math>\lambda</math>-sensor is active</li> <li>• Second <math>\lambda</math>-sensor is active</li> <li>• Third <math>\lambda</math>-sensor is active</li> <li>• Modelled exhaust gas temp. In range</li> </ul>	{Quick pass	Quick pass}	=> Quick pass
<ul style="list-style-type: none"> <li>• First <math>\lambda</math>-sensor is active</li> <li>• Second <math>\lambda</math>-sensor is active</li> <li>• Modelled front exhaust gas temp. In range</li> <li>• Modelled main exhaust gas temp. In range</li> <li>• Exhaust- gas mass flow in range</li> <li>• Exhaust- gas mass dynamic in range</li> </ul>	Measureme nt of OSC- calculation		
<ul style="list-style-type: none"> <li>• First <math>\lambda</math>-sensor is active</li> <li>• Second <math>\lambda</math>-sensor is active</li> <li>• Third <math>\lambda</math>-sensor is active</li> <li>• Modelled front exhaust gas temp. In range</li> <li>• Modelled main exhaust gas temp. In range</li> <li>• Exhaust- gas mass flow in range</li> <li>• Exhaust- gas mass dynamic in range</li> </ul>		Measureme nt of OSC- calculation	
<ul style="list-style-type: none"> <li>• First <math>\lambda</math>-sensor is active</li> <li>• Third <math>\lambda</math>-sensor is active</li> <li>• Modelled front exhaust gas temp. In range</li> <li>• Modelled main exhaust gas temp. In range</li> <li>• Exhaust- gas mass flow in range</li> <li>• Exhaust- gas mass dynamic in range</li> </ul>			Measurement of OSC- calculation

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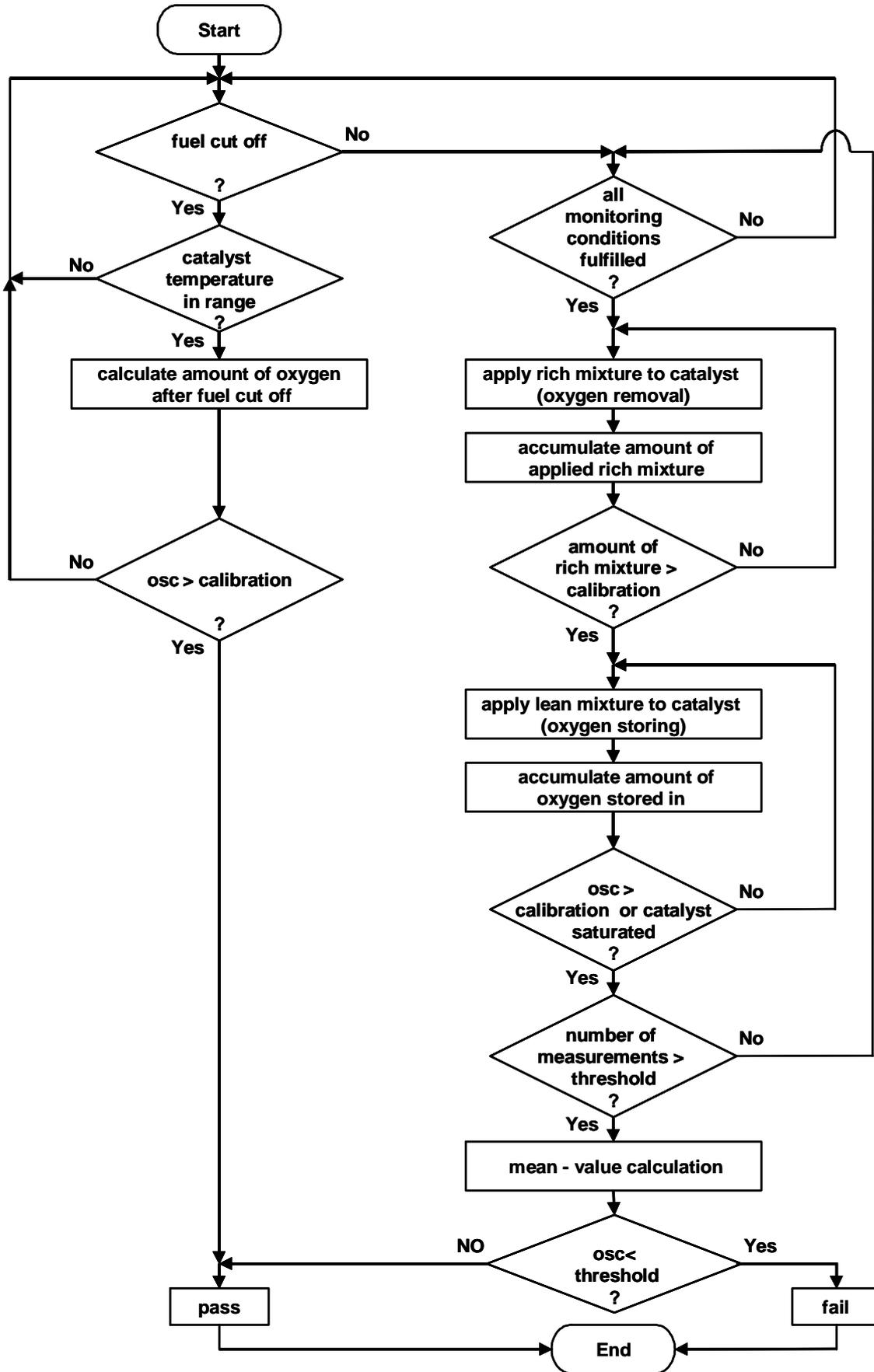
If the secondary parameters for the different catalyst portions are met at the same time, the diagnostic functions can run simultaneously.

According to table 1 the following result combinations are described in table 2.

Table 2: Results, which can be obtained after the diagnosis of the different catalyst volumes

<b>Front catalyst</b>	<b>Main catalyst Or Catalyst system</b>	<b>Result</b>
Quick pass	Quick pass	Both = pass
Quick pass	Measurement of OSC- calculation < threshold	front catalyst = pass main catalyst = Fail
Quick pass	Measurement of OSC- calculation > threshold	Both = pass
Measurement of OSC- calculation < threshold	Quick pass	front catalyst = Fail main catalyst = passe
Measurement of OSC- calculation > threshold	Quick pass	Both = pass
Measurement of OSC- calculation < threshold	Measurement of OSC- calculation < threshold	Both = fail
Measurement of OSC- calculation > threshold	Measurement of OSC- calculation > threshold	Both = pass
Measurement of OSC- calculation > threshold	Measurement of OSC- calculation < threshold	front catalyst = pass main catalyst = fail
Measurement of OSC- calculation < threshold	Measurement of OSC- calculation > threshold	front catalyst = fail main catalyst = pass

.01.02.03 Flow Chart Catalyst Monitoring



**.02.00.00 HEATED CATALYST MONITORING**

Not applicable

**.03.00.00 MISFIRE MONITORING**

**.03.00.01 General Description**

The method of engine misfire detection is based on evaluating the engine speed fluctuations.

In order to detect misfiring at any cylinder, the torque of each cylinder is evaluated by metering the time between two ignition events, which is a measure for the mean value of the speed of this angular segment. This means, a change of the engine torque results in a change of the engine speed.

Additionally the influence of the load torque will be determined. When the mean engine speed has been measured, influences caused by different road surfaces have to be eliminated (e.g. pavement, pot holes etc.).

This method consists of the following main parts:

- Correction of normal changes of engine rpm and engine load
  
- Data acquisition, adaptation of sensor wheel and typical engine behaviour is included
  
- Calculation of engine roughness
  
- Comparison with a threshold depending on operating point
  
- Fault processing, counting procedure of single or multiple misfire events

### .03.01.02 Monitoring function description

#### Data acquisition

The duration of the crankshaft segments is measured continuously for every combustion cycle and stored in a memory.

#### Sensor wheel adaptation

Within defined engine speed and load ranges the adaptation of the sensor wheel tolerances and the typical engine behaviour is carried out, if no misfire events are detected.

With progressing adaptation the sensitivity of the misfire detection is increasing.

The adaptation values are stored in a non-volatile memory and taken into consideration for the calculation of the engine roughness.

#### Misfire detection

The following operating steps are performed for each measured segment, corrected by the sensor wheel adaptation.

#### Calculation of the engine roughness

The engine roughness is derived from the differences of the segment's duration.

Different statistical methods are used to distinguish between normal changes of the segment duration and the changes due to misfiring.

#### Detecting of multiple misfiring

If several cylinders are misfiring (e.g. alternating one combustion/one misfire event), the calculated engine roughness values may be so low, that the threshold is not exceeded during misfiring and therefore, misfiring would not be detected.

Based on this fact, the periodicity of the engine roughness value is used as additional information during multiple misfiring. The engine roughness values are filtered and a new multiple filter value is created. If this filter value increases due to multiple misfiring, the roughness threshold is decreased. By applying this strategy, multiple misfiring is detected reliably.

#### Calculation of the engine roughness threshold value

The engine roughness threshold value consists of the base value, which is determined by a load/speed dependent map.

During warm-up, a coolant-temperature-dependent correction value is added. In case of multiple misfiring the threshold is reduced by an adjustable factor.

Without sufficient sensor wheel adaptation the engine roughness threshold is limited to a speed dependent minimum value.

A change of the threshold towards a smaller value is limited by a variation of filter value (low pass filter).

## **Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

Determination of misfiring

### Random misfire

Comparing the engine roughness threshold value with the engine roughness value performs misfire detection.

If the engine roughness value is greater than the roughness threshold value a single misfire is detected. With this misfire determination it is possible to identify misfiring cylinders individually.

### Random misfire without valid adaptation

To eliminate the influence of the missing flywheel adaptation each engine roughness value is compared with that one on the same flywheel segment on the intermittent revolution. Therefore single misfire events are detected reliable without determination of the flywheel tolerances.

### Continuous misfire on one or multiple cylinders

To avoid noise effects, all engine roughness values are low pass filtered and the detection threshold is corrected by the mean value of the filters. Therefore the amplitude to noise ratio improves and the sensitivity for misfire detection of continuous misfiring cylinders increases.

## **Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

### **Statistics, Fault processing:**

Within an interval of 1,000 crankshaft revolutions, the detected number of misfiring events is totalled for each cylinder. If the sum of cylinder fault counters exceeds a predetermined value, a fault code for emission relevant misfiring is preliminary stored after completion of the first interval after engine has been started or the forth interval during a driving cycle where misfire has been detected.

In the case of misfire detection for one cylinder, the fault is determined by a cylinder selective fault code otherwise the fault code for multiple misfire will be stored additionally.

Within an interval of 200 crankshaft revolutions, the detected numbers of misfire events is weighted and totalled for each cylinder.

The weighting factor is determined by a load/speed dependent map.

If the sum of cylinder fault counters exceeds a predetermined value, the fault code for indicating catalyst damage relevant misfiring is stored and the MIL is illuminated with "on/off"-sequence once per second (blinking).

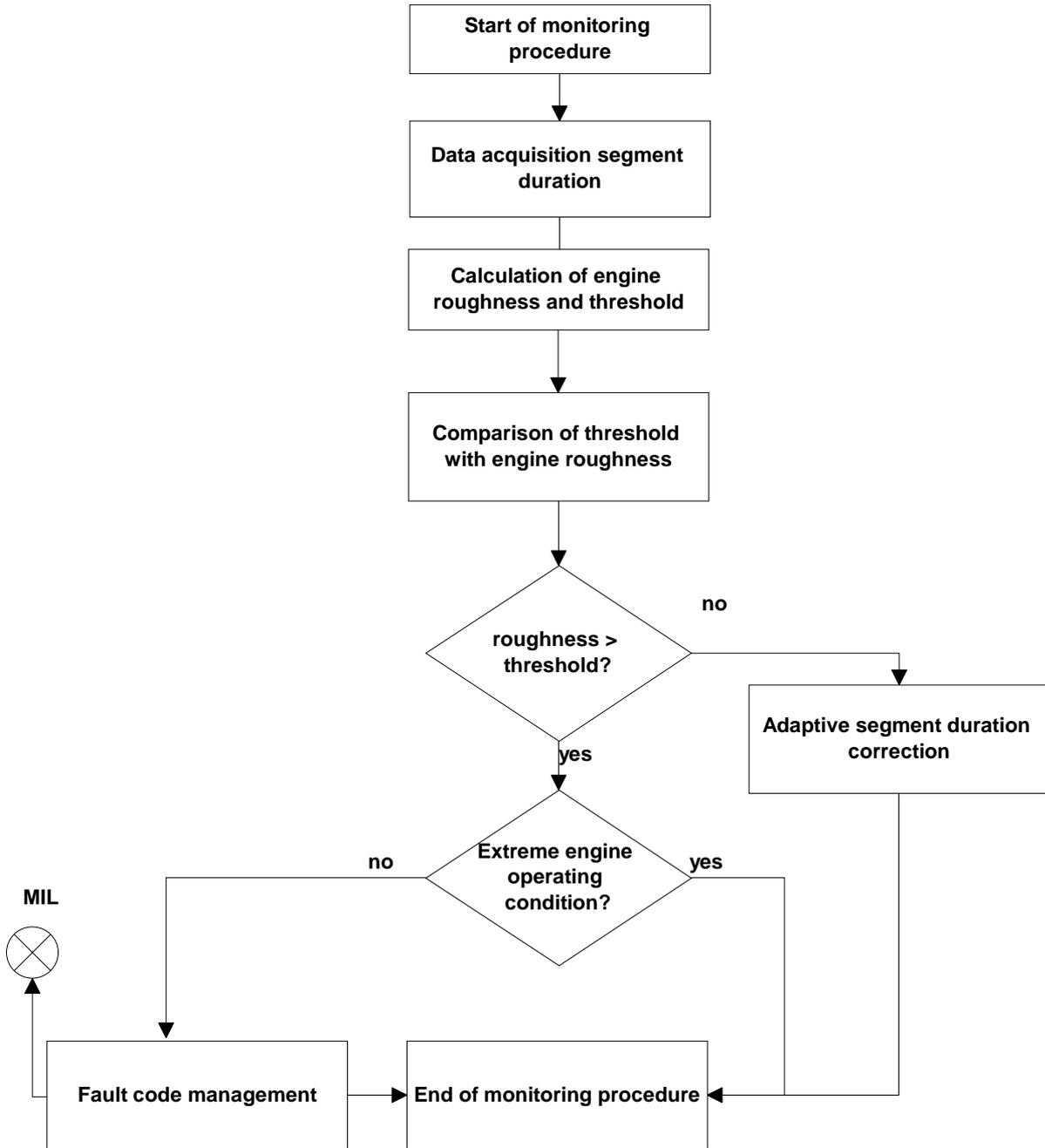
In case of misfire detection for one cylinder the fault is determined by a cylinder selective fault code otherwise the fault code for multiple misfiring will be stored additionally.

If catalyst damaging misfire does not occur any longer during the first driving cycle, the MIL will return to the previous status of activation (e.g. MIL off) and will remain illuminated continuously during all subsequent driving cycles if catalyst related misfire is detected again. However all misfire events where the catalyst can be damaged are indicated by a blinking MIL. If catalyst damage is not detected under similar conditions in the subsequent driving cycle the temporary fault code will be deleted.

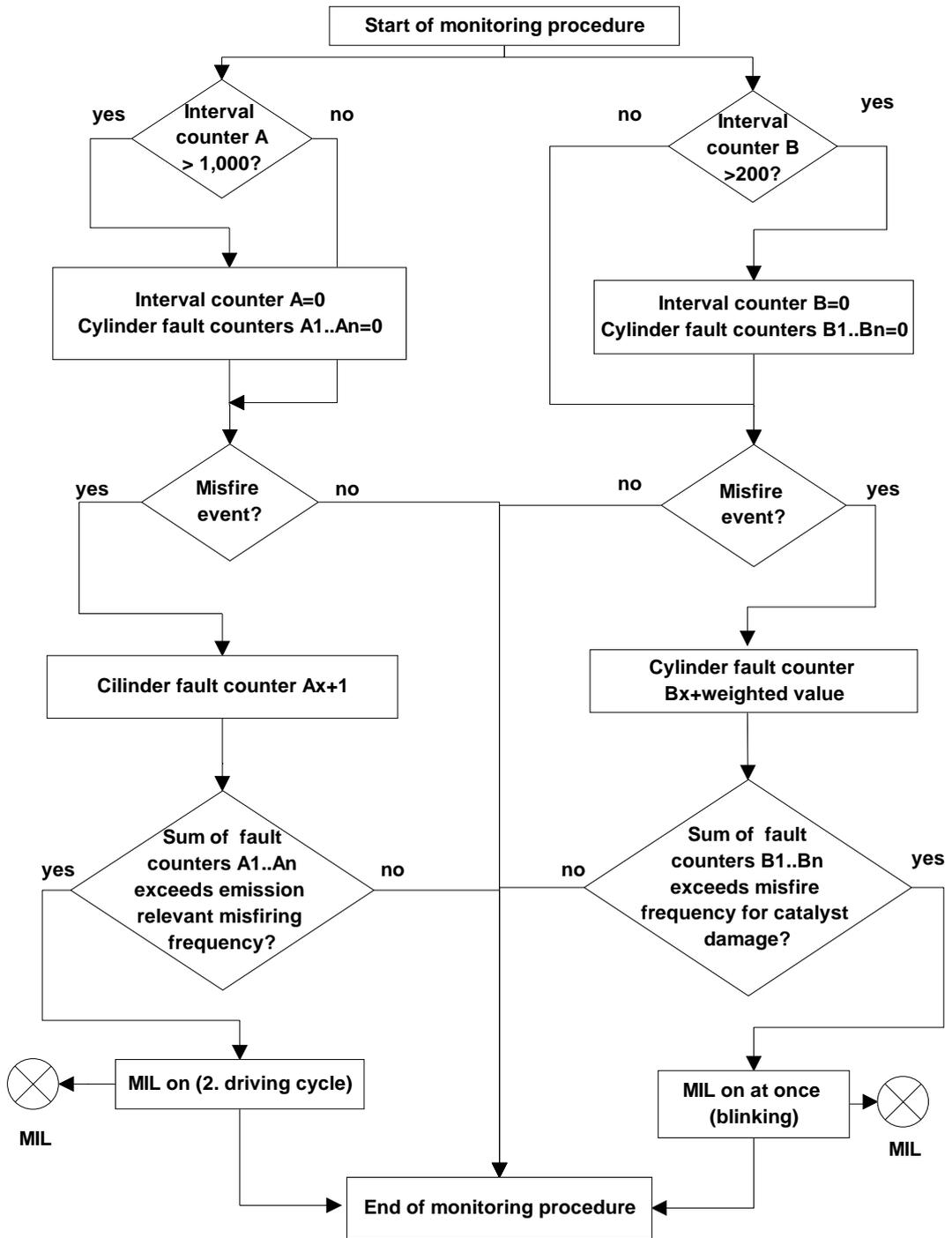
In the case of catalyst related misfire, the Lambda closed loop system is switched to open-loop condition according to the basic air/fuel ratio calculation ( $\text{Lambda}=1$ ).

All misfire counters are reset after each interval.

.03.00.03 Chart(s) and Flow Chart(s)



Paths for misfire and catalyst damaging misfire rate



**.04.00.00 EVAPORATIVE SYSTEM DIAGNOSIS**

**.04.01.00 Leakage Check**

**.04.01.01 General description**

The leakage diagnosis procedure is a pressure check of the EVAP system.

In order to perform the check, the EVAP system will be sealed and pressure applied by the leakage diagnosis pump (LDP). The pressure variation time is analysed by the ECM.

**.04.01.02 Monitoring function description**

The diagnosis procedure consists of the following steps:

**1. Tank pressure check**

The first step of leakage diagnostics is the pressure check of fuel tank system by testing the reed switch. In case of an open reed switch, the fuel tank system has sufficient pressure for the sealed check and no further pressure has to be supplied to the fuel tank system by the LDP. The diagnosis is waiting until the EVAP purge valve is opened in order to purge the carbon canister. In case the reed switch remains open or the reed switch stuck open, the reed switch is defective.

In the case the reed switch is closed, the LDP is switched on in order to supply pressure to the fuel tank system and the diagnostic is continued with the step 2 to 3 (as described below).

**2. LDP Self-check procedure**

**Closed check**

LDP control is disabled and the reed switch has to be closed otherwise the reed switch is defective.

**Close to open check**

LDP control is switched on once and the diaphragm has to move to the upper position. The time is measured between closed and open position of diaphragm detected by the reed switch. When the final upper position of diaphragm is reached in a certain time, then the check will be passed.

**3. Leak check of EVAP system**

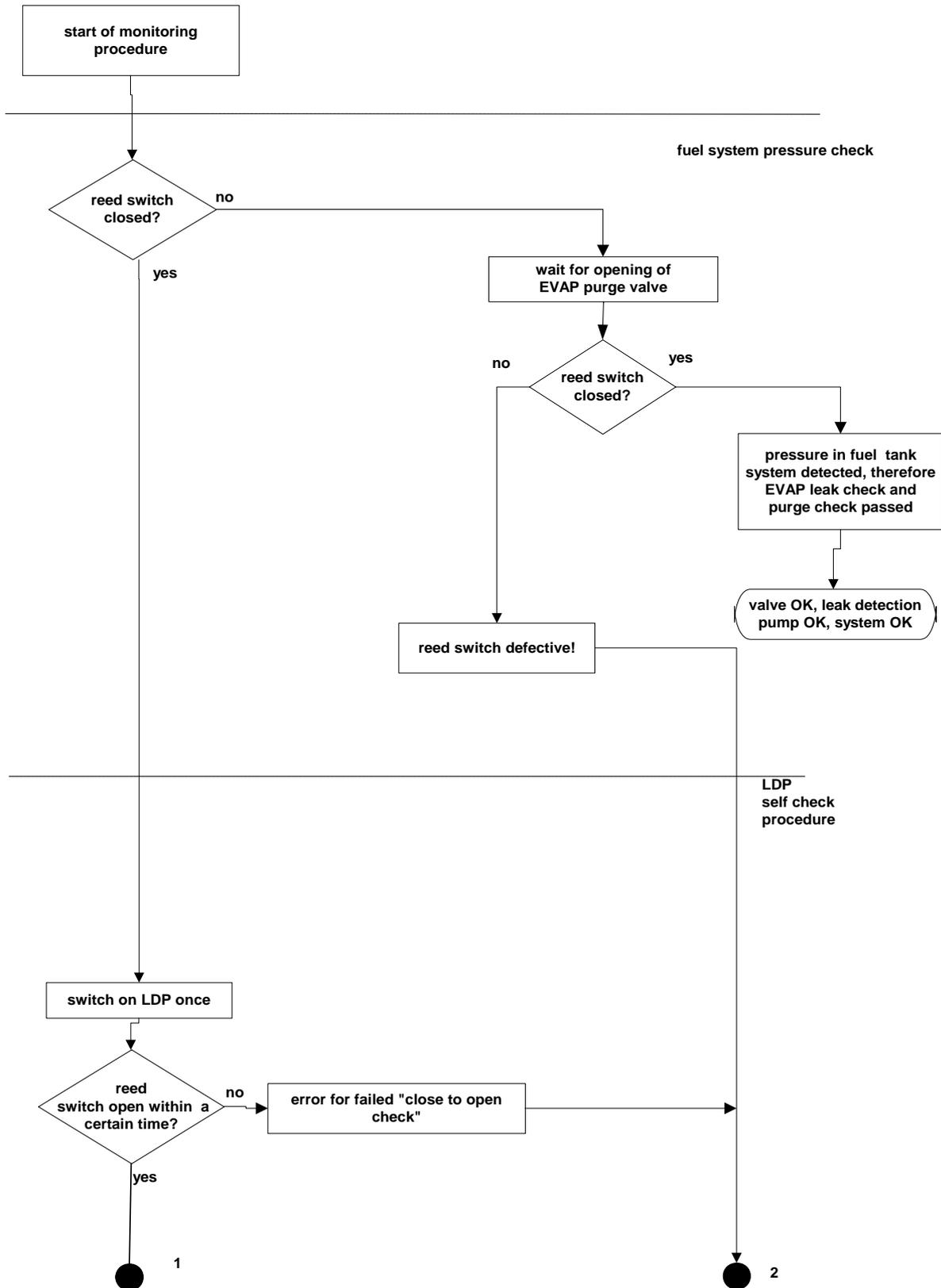
**Fast pulse**

After the self check procedure, the LDP control supplies pressure to the fuel tank system with a pressure dependent number of compression strokes in a certain time. In order to supply pressure to the fuel tank system, the LDP can perform compression strokes in several attempts.

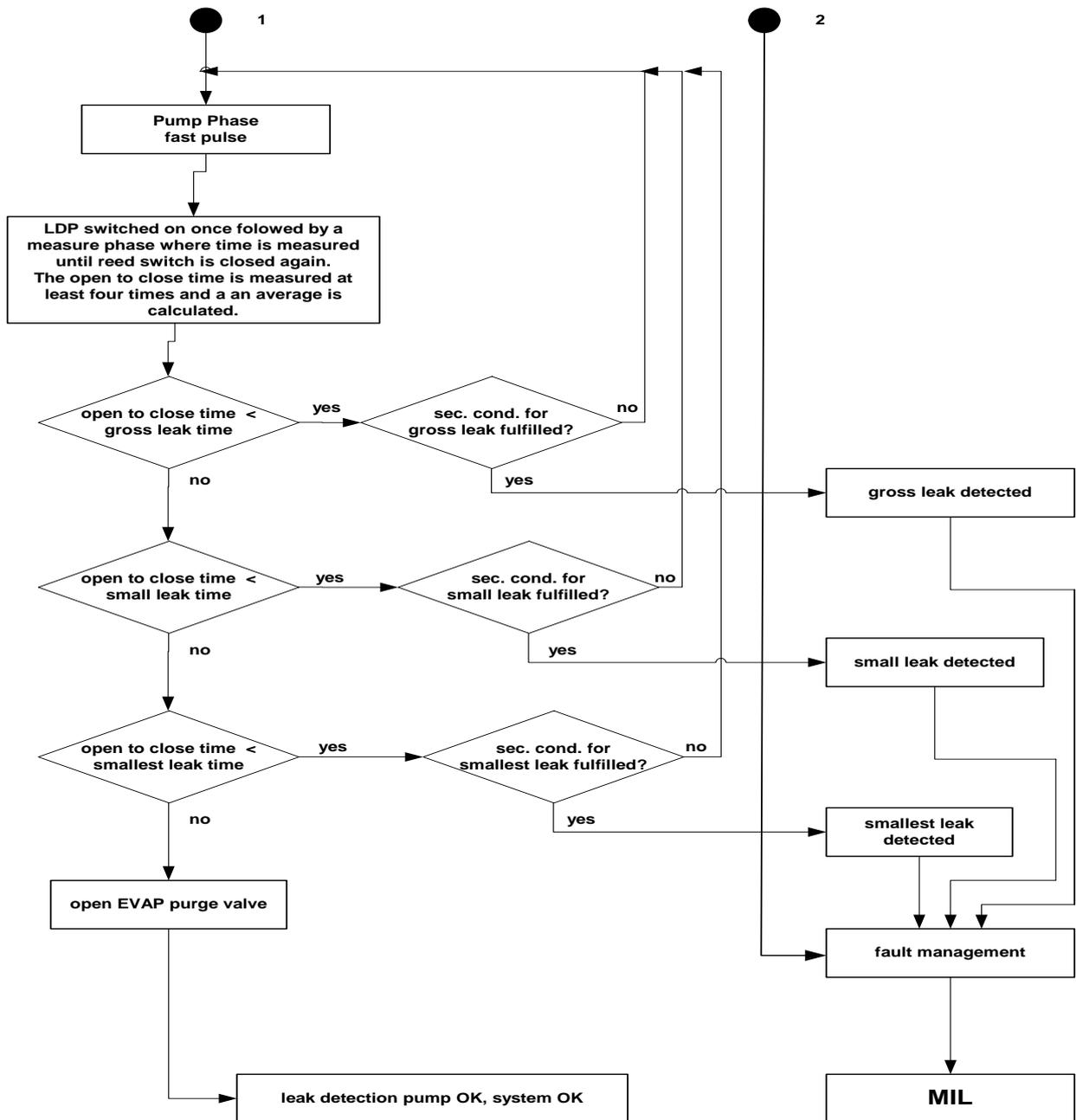
**EVAP system sealed check, measure stroke and measure phase**

The decrease of fuel tank pressure is measured via time of diaphragm movement followed by a compression stroke. Within a certain time, the LDP control is determined within at least four measurement strokes. The averaged time is a measure for the tightness of fuel tank system.

.04.01.03 Chart(s) and flow chart(s)



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**.04.02.00** ..... **Purge Check**

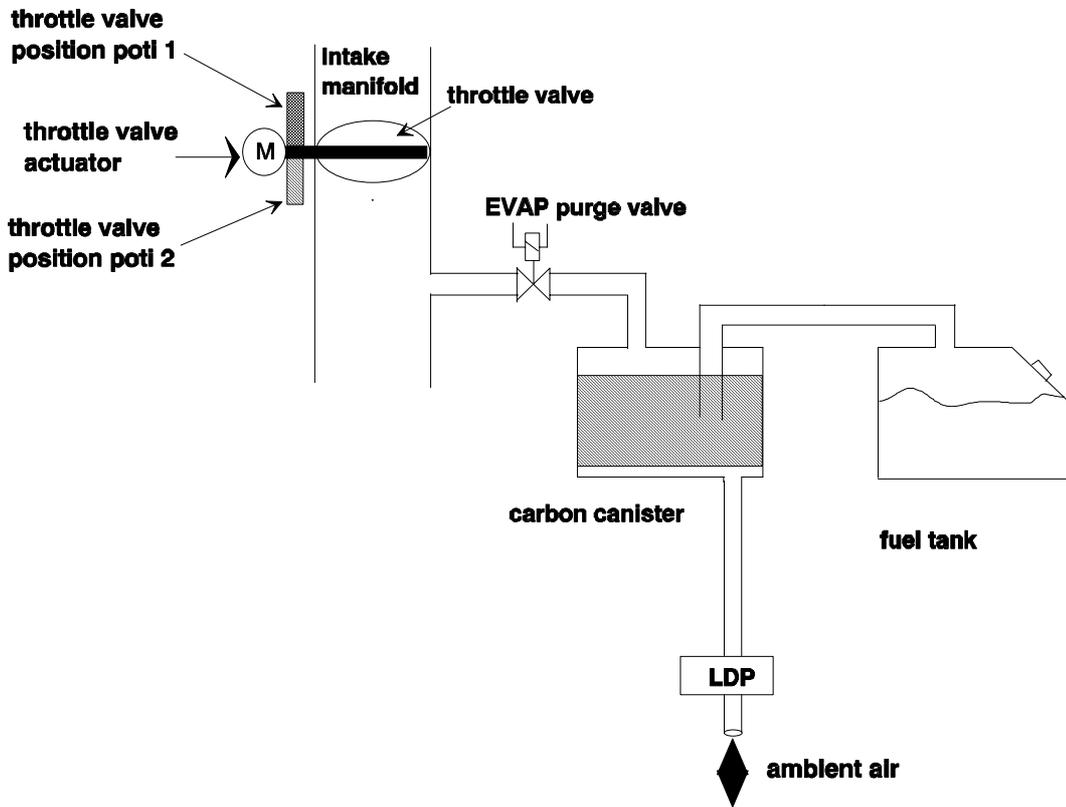
**.04.02.01**    **General description**

The purge flow through the EVAP Purge Valve is checked when the vehicle is at rest during an idle condition and the Lambda controller is active. The EVAP Purge Valve is opened while monitoring the Lambda controller and the airflow through the throttle unit.

For rich or lean mixture through the EVAP Purge Valve:

Flow through the EVAP Purge Valve is assumed as soon as the Lambda controller compensates for a rich or lean shift.

After this procedure the EVAP Purge Valve is reset and the diagnosis is completed.

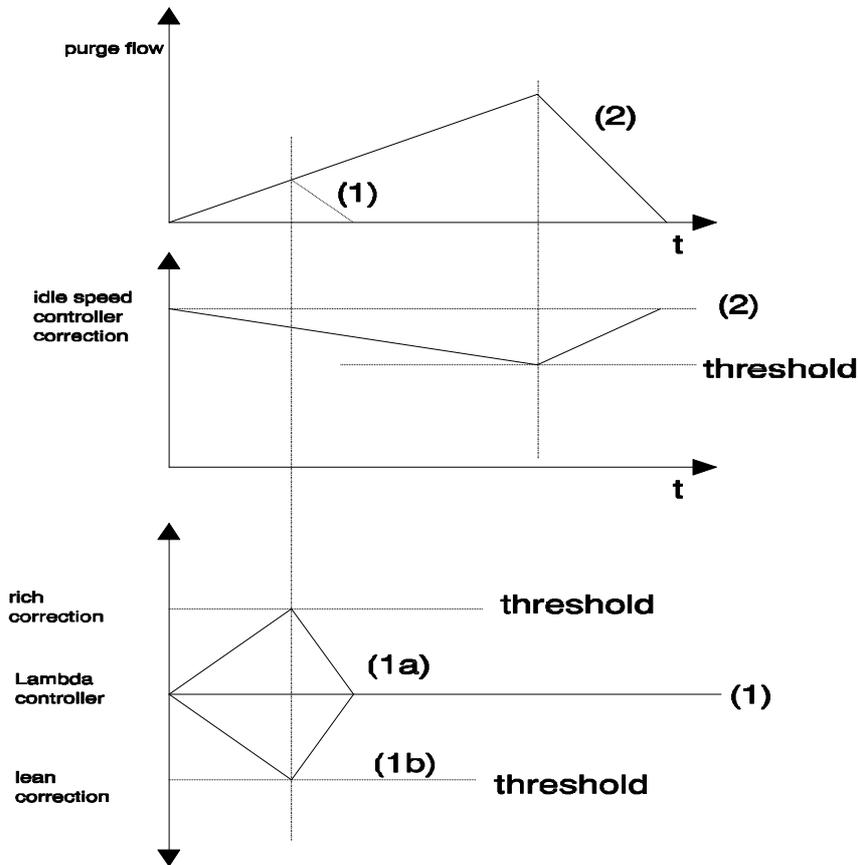


**.04.02.02 Monitoring function description**

**For stoichiometric mixture flow through the EVAP Purge Valve:**

In this case, the Lambda controller does not need to compensate for a deviation. However, when the EVAP Purge Valve is completely opened, the cylinder charge increases significantly. Therefore, flow through the throttle unit must be decreased in order to maintain the desired idle speed. Flow through the EVAP Purge Valve is assumed when the flow through the throttle unit is reduced by idle control. If both mixture compensation and reduction of the airflow through the throttle unit does not occur for two diagnosis cycles, then a defective EVAP Purge Valve is assumed and the MIL is illuminated.

**.04.02.03 Chart(s) and flow chart(s)**



**Open purge valve and monitor effects of purge flow:**

- (1) **Lambda purge flow <> 1:** Abortion if fresh air (1a) or HC (1b) detected
- (2) **Lambda purge flow = 1:** Throttle unit actuator will reduce the flow rate through the throttle due to additional flow through purge valve

**MIL will be illuminated if none of said effects occurs.**

.05.00.00      SECONDARY AIR SYSTEM MONITORING

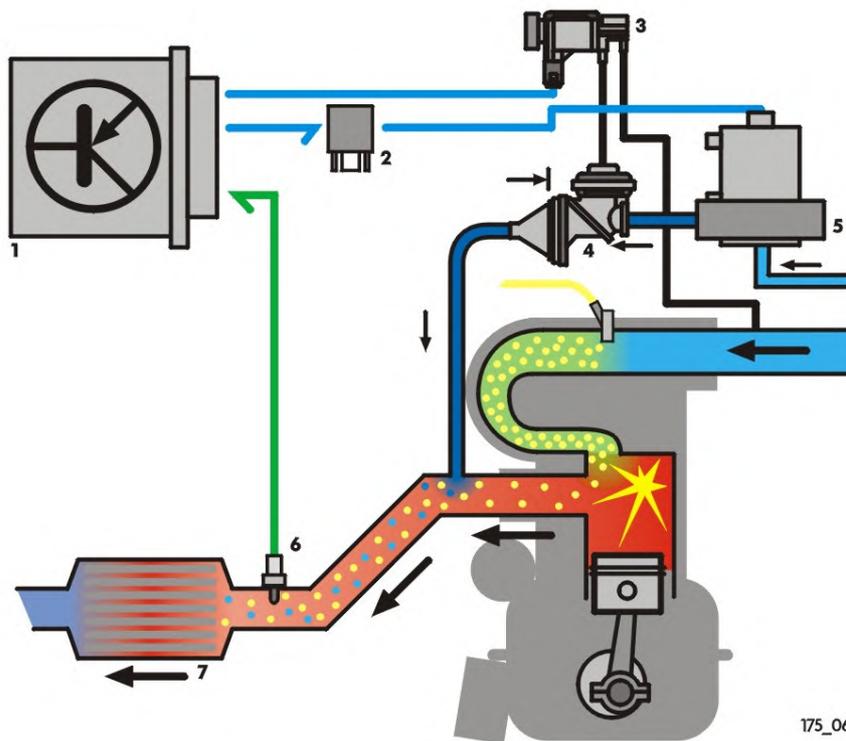
.05.01.00      Via lambda deviation

**.05.01.01**      **General Description**

After cold start condition (e.g. 5 .. 40°C) the Air system blows for a certain time air into the exhaust manifold. The exhaust gases will be enriched with oxygen and post combustion of HC and CO occurs. By this exothermic reaction the exhaust system will be heated and the time to reach the light-off temperature of the catalyst will be accelerated.

Principal sketch and main components of Air System: (example 4 cyl. Engine)

- ECM;
- Air pump relay
- Air valve (solenoid valve)
- Air valve (vacuum controlled)
- AIR pump;
- O2 Sensor;



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## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### .05.01.02 Monitoring Structure

The following table shows an overview of the used function and monitor strategy for all test groups:

Test Group	Engine	Standard	Via Lambda deviation				Via exhaust temperature sensor				
			Passive check		Active check		Passive check		Active check		
			Functional	Flow Check	Functional	Flow Check	Functional	Flow Check	Functional	Flow Check	
5ADXV01.8342	1.8T I-4 Turbo long.	Bin 8	-	-	Yes	-	-	-	-	-	-
5ADXV01.8356	1.8T I-4 Turbo	Bin 8	yes	-	yes	-	-	-	-	-	-
5ADXV01.8346	1.8T I-4 Turbo	LEV I	yes	-	yes	-	-	-	-	-	-
5VWXV02.0223	2.0I I-4	LEV II	-	-	Yes	-	-	-	-	-	-
5VWXV02.0224	2.0I I-4	ULEV II	-	-	Yes	-	-	-	-	-	-
5VWXV02.0227	2.0I I-4	PZEV	-	-	yes	-	yes	-	-	-	-
5VWXV02.0240	2.0I I-4 Turbo	ULEV II	-	-	Yes	-	-	-	-	-	-
5ADXV02.8334	2.8I V6 - 2 bank	LEV I	te	-	yes	-	-	-	-	-	-
5ADXV03.0344	3.0I V6 - 2 bank	LEV II			yes	yes	-	-	-	-	-
5ADXV04.2345	4.2I V8 - 2 bank	LEV I	yes	-	yes	-	-	-	-	-	-
5ADXT04.2348	4.2I V8 - 2 bank	Bin 10	yes	-	yes	-	-	-	-	-	-
5ADXV02.7343	2.7I V6T - 2 bank	LEV I	yes	-	yes	-	-	-	-	-	-
5VWXT03.2225	3.2 VR6 - 2 bank	LEV II	-	-	Yes	-	-	-	-	-	-
5VWXV02.8228	2.8 VR6 - 2 bank	LEV I	-	-	Yes	-	-	-	-	-	-
5VWXV03.2220	3.2 VR6 - 2 bank	LEV I	-	-	Yes	-	-	-	-	-	-
5VWXV04.0229	4.0I W8 – 2 bank	LEV I	-	-	Yes	-	-	-	-	-	-
5VWXV06.0221	6.0I W12 – 2 bank	LEV I	-	-	Yes	-	-	-	-	-	-
5VWXV06.0501	6.0I W12T – 2 bank	LEV I	-	-	Yes	-	-	-	-	-	-

The monitor of the secondary air system distinguish between two functions:

- a) Passive monitoring function will be carried out during normal secondary air injection  
While engine is cold started and
- b) Active monitoring function will be activated later during the driving cycle, if the passive Monitoring function has not a pass result.

At idle state or under part load engine condition, the secondary air pump is switched on and the valve opens either by pressure of the pump or vacuum operated by switching to “open”, causing an increase in the air fuel ratio. The Oxygen Sensor control function (closed loop) enriches the mixture consisting of exhaust gas of the engine and secondary air until the Lambda integrator signal will meet a predetermined value (functional or flow check).

## **Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

Check Conditions

### Passive Monitoring Function

To start the passive monitoring function, following conditions have to be satisfied:

Oxygen sensor readiness  
No engine restart (thermal energy introduced)  
A certain time after engine start  
Engine has been cold started  
No output stage error from secondary air pump relay

### Active Monitoring Function

To start the active monitoring function several conditions have to be satisfied:

No result or no "pass" result from passive monitoring function available.  
Engine running at idle  
Closed loop condition of the Lambda-control  
Monitoring function not done before (for pump protection)  
No output stage error from secondary air pump relay

Furthermore, if the diagnosis has already been started and one of the conditions has not been satisfied continuously, the process will be interrupted.

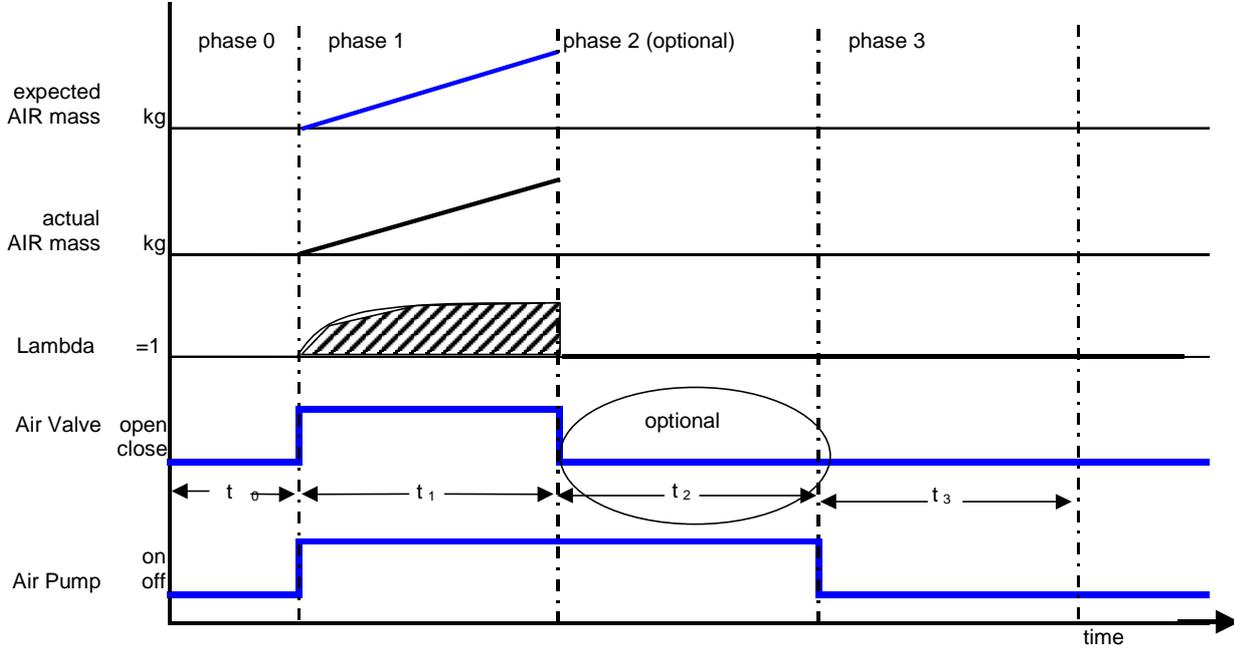
The following conditions have to be fulfilled additionally:

All adaptations of the air/fuel system are inhibited  
The Lambda controller has been stabilized (waiting for several transients of the oxygen sensor signal)  
The actual Lambda controller value has been stored  
In case of an interrupt of diagnosis, the monitor can several time started again (different for each test group; see overview) during the same driving cycle if the monitor conditions are met.

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

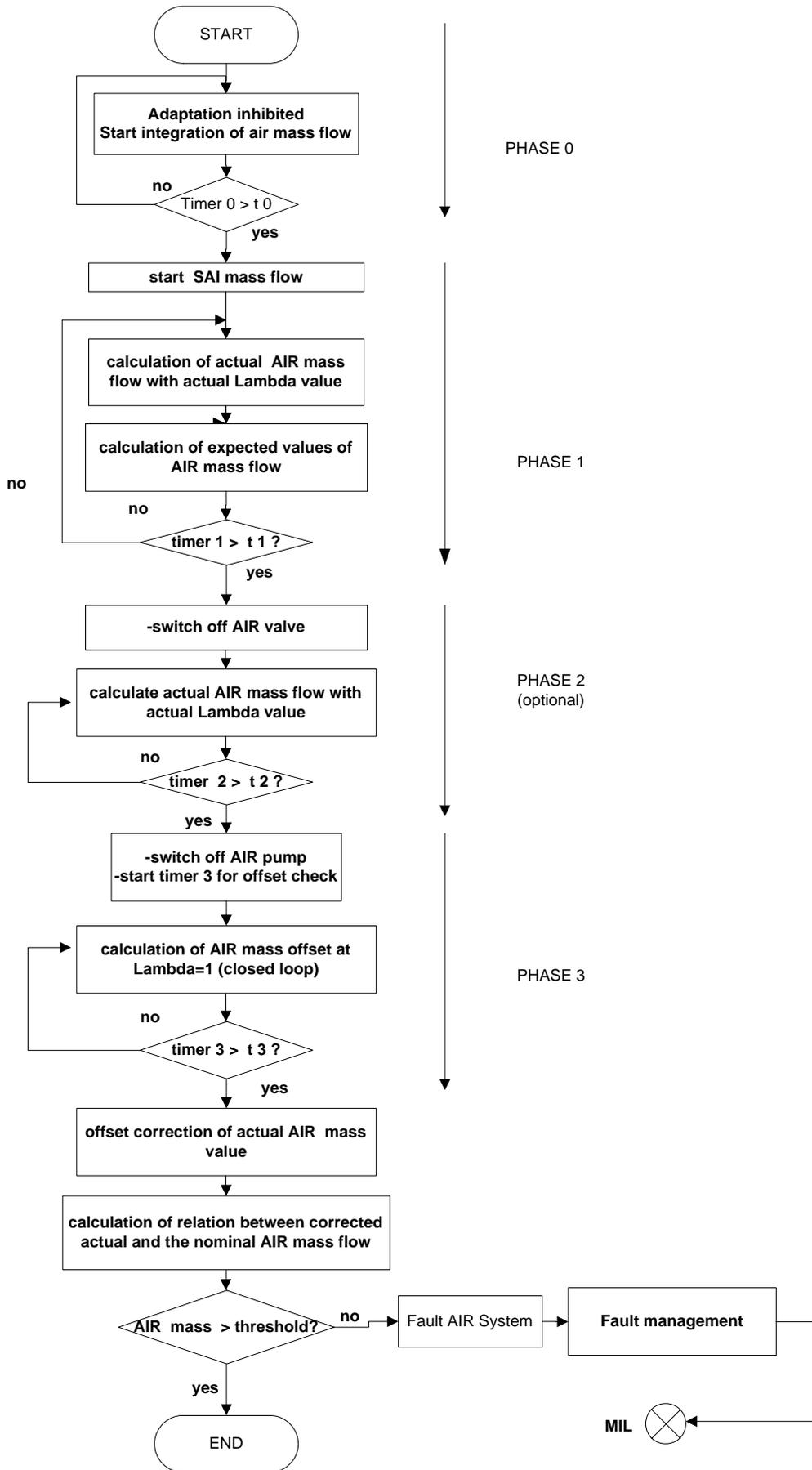
### .05.01.03 Chart(s) and flow chart(s)

Following charts shows the phases of the AIR monitoring via lambda deviation for passive and active monitoring.



AIR system monitoring	
DTC's	See summary table
Sensors OK	ECTS, Front O2S
Secondary Parameter	See summary table
Monitor execution	Passive check during normal operation
Threshold	Malfunction criteria from summary table as relation between actual and expected AIR.

# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy



## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### .05.02.00 Via exhaust temperature sensor

#### **.05.02.01 General Description**

After cold start condition (e.g. 5 .. 40°C) the Air system blows for a certain time air into the exhaust manifold. The exhaust gases will be enriched with oxygen and post combustion of HC and CO occurs. By this exothermic reaction the exhaust system will be heated and the time to reach the light-off temperature of the catalyst will be accelerated.

Additional to the principal sketch above, those systems using an exhaust temperature sensor as an indicator of AIR mass.

#### **.05.02.02 Monitor function description**

##### Passive monitoring function

During normal secondary air injection the secondary air is indirect monitored via exhaust temperature using an exhaust temperature sensor. The measured exhaust temperature will be compared with modeled target temperatures contained in a map within ECM. After the secondary air injection ECM is calculating the amount of introduced thermal energy additionally. As long as the temperature sensor shows an increase in exhaust gas temperature and the thermal energy introduced (calculated by air mass times injected fuel), the secondary system will pass the monitor. No further active diagnostic will be performed.

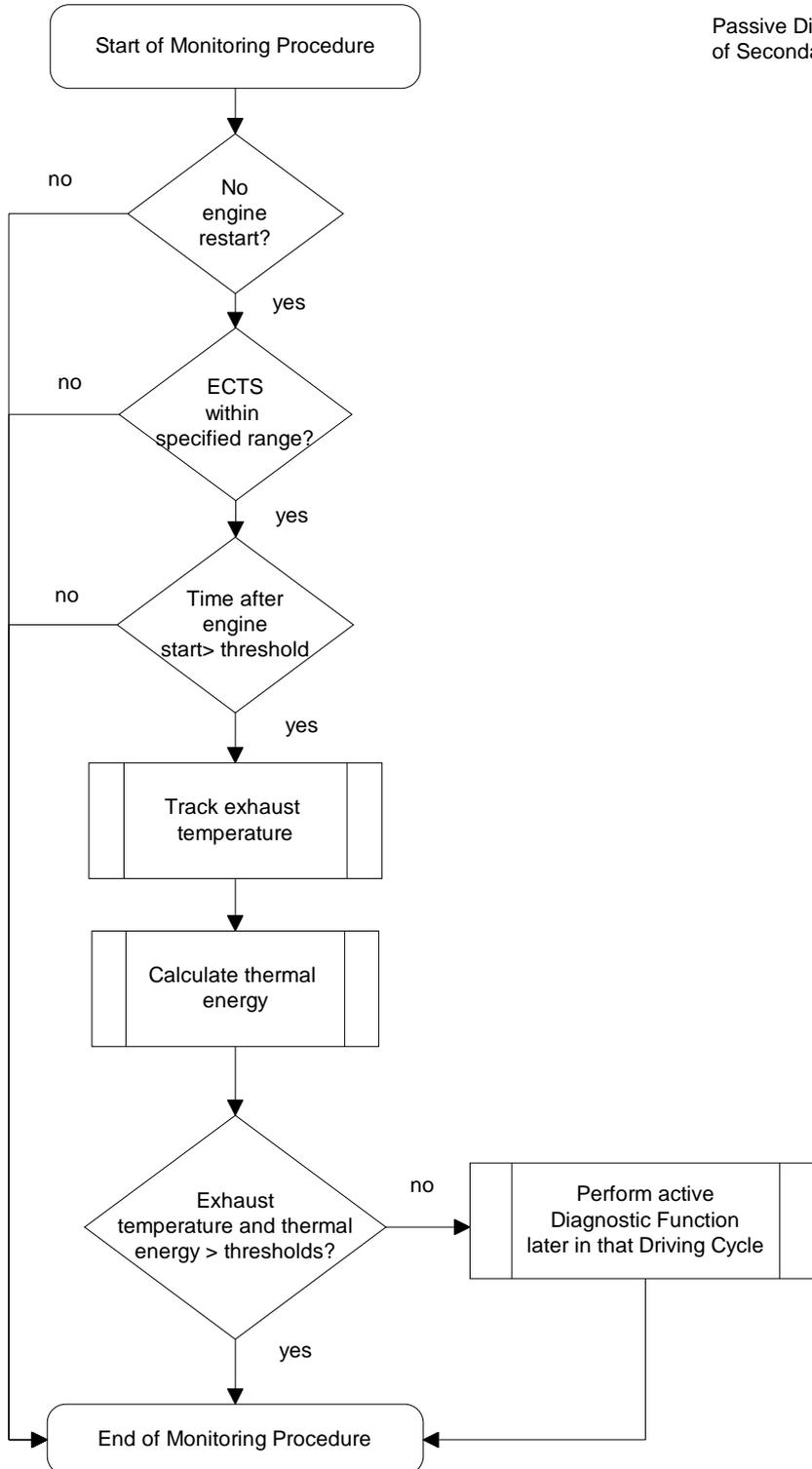
If one of the expected conditions fails, e.g. the temperature sensor is not showing an increase of temperature or the thermal energy introduction is below an expected threshold, the active monitoring function will be carried out later in that driving cycle.

<b>AIR System monitoring (via exhaust temperature sensor)</b>	
DTC's	See summary table
Sensors OK	ECTS, Front O2S
Secondary Parameter	See summary table
Monitor execution	Passive check during normal operation
Threshold	Decision criteria for pass condition from summary table as relation between actual and expected AIR.

.05.02.03

Chart(s) and flow chart(s)

Passive Diagnostic  
of Secondary Air System



.06.00.00      **Fuel System Monitoring**

**.06.00.01**      **General Description**

**Mixture Pilot Control**

The airflow sucked in by the engine and the engine speed is measured. These signals are used to calculate an injection signal. This mixture pilot control follows fast load and speed changes.

**Lambda-controller**

The ECM compares the Oxygen sensor signal upstream the catalyst with a reference value and calculates a correction factor for the pilot control.

**.06.00.02**      **Monitoring function description**

**Adaptive pilot control**

Drifts and faults in sensors and actuators of the fuel delivery system as well as unmeasured air leakage influence the pilot control. The controller corrects amplitudes increases. If there are different correction values needed in different load speed ranges, a certain time passes until the correction is complete. The correction values will be determined in three different ranges.

**Fuel trim**

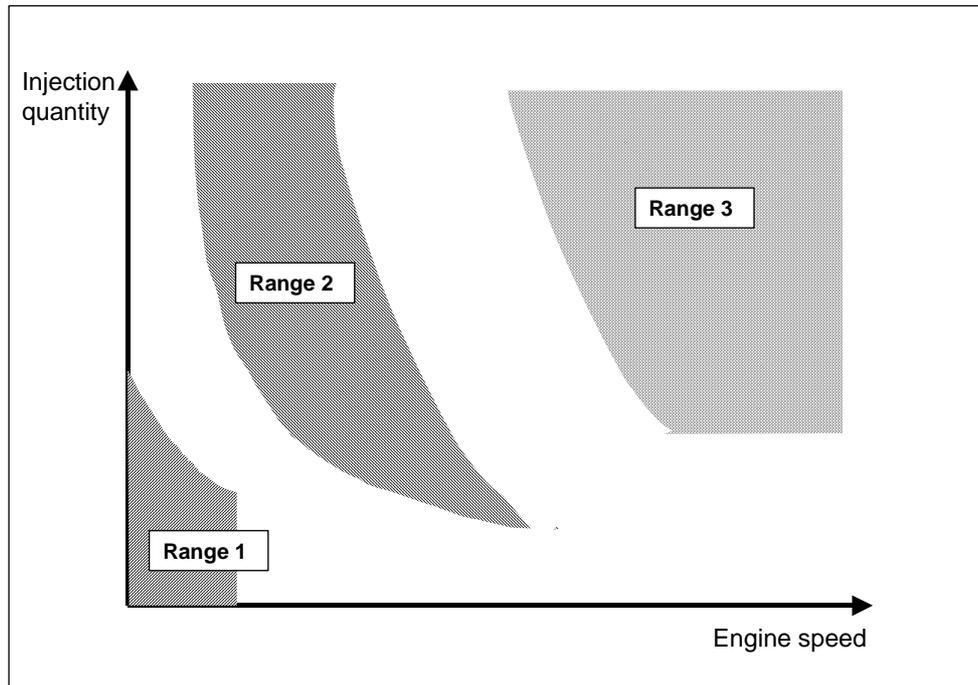
The basic air/fuel ratio control using the signal from the front O2 sensors(s) is corrected by an adaptation calculation. This adaptation results in a factor, which is applicable for the whole working range. (e.g. 20%)

A further trim control based on the signal(s) from the rear O2 sensor(s) is correcting the adaptation factor. Therefore this trim control is working in the same way in the whole range.

If the trim control reaches the allowed limit (e.g. 2%) the fault code for fuel delivery trim control is set.

Any deviation from the characteristic curve of oxygen sensor upstream catalyst due to poison will be detected by the control loop downstream catalyst.

.06.00.03 Chart(s) and flow chart(s)



Lambda deviations in **range 1** are compensated by an additive correction value multiplied by an engine speed term. This creates an additive correction per time unit.

Lambda deviations in **range 2** are compensated by multiplication of a factor.

Lambda deviations in **range 3** are compensated by multiplication of a factor (optional depending on individual calibration).

A combination of all two (three) ranges will be correctly separated and compensated.

Each value is adapted in its corresponding range only. But each adaptive value corrects the pilot control within the whole load/speed range by using a linear interpolation formula. The stored adaptive values are included in the calculation of the pilot control just before the closed loop control is active.

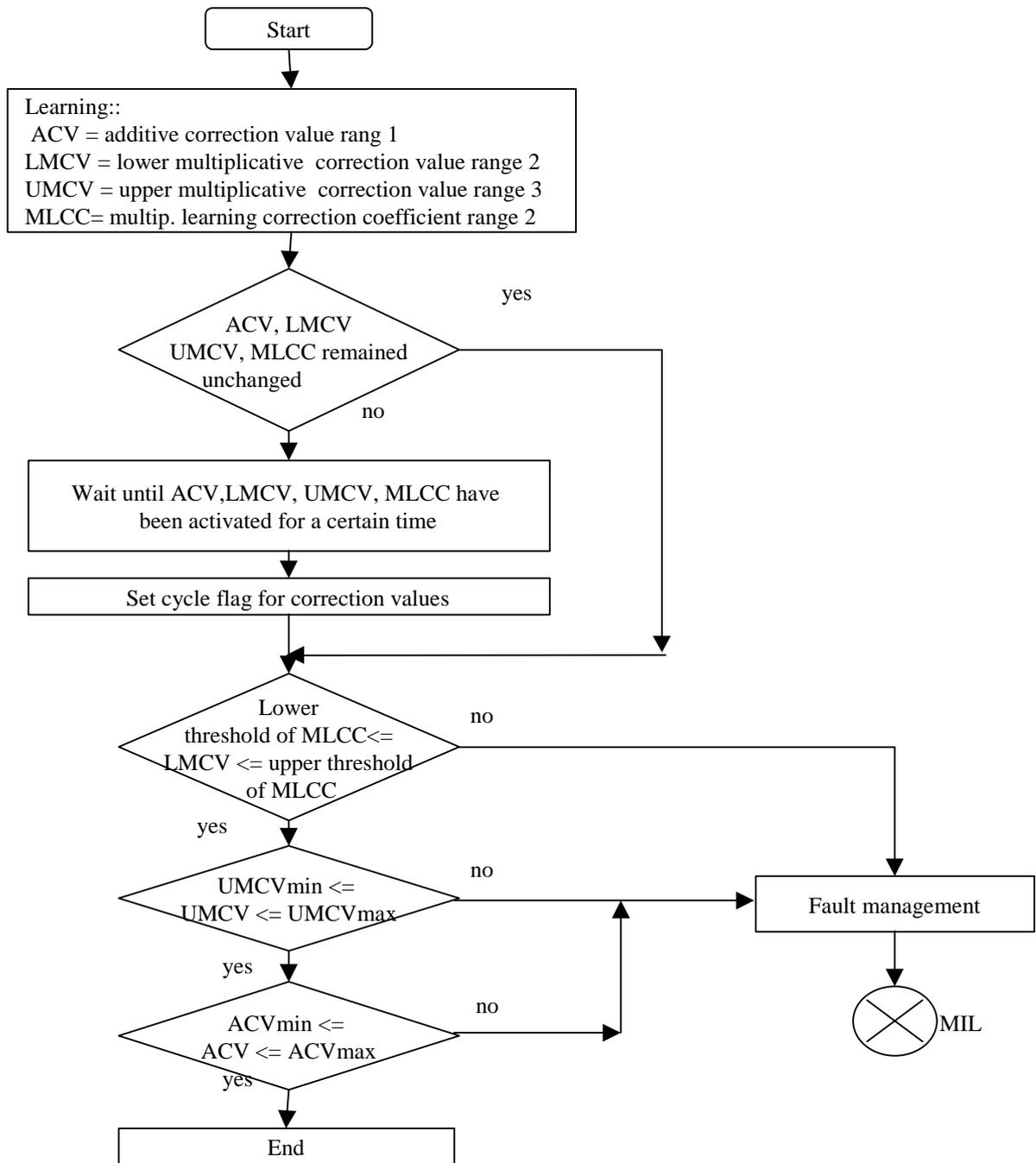
Diagnosis of the fuel delivery system

Faults in the fuel delivery system can occur which cannot be compensated for by the adaptive pilot control.

In this case, the adaptive values exceed a predetermined range.

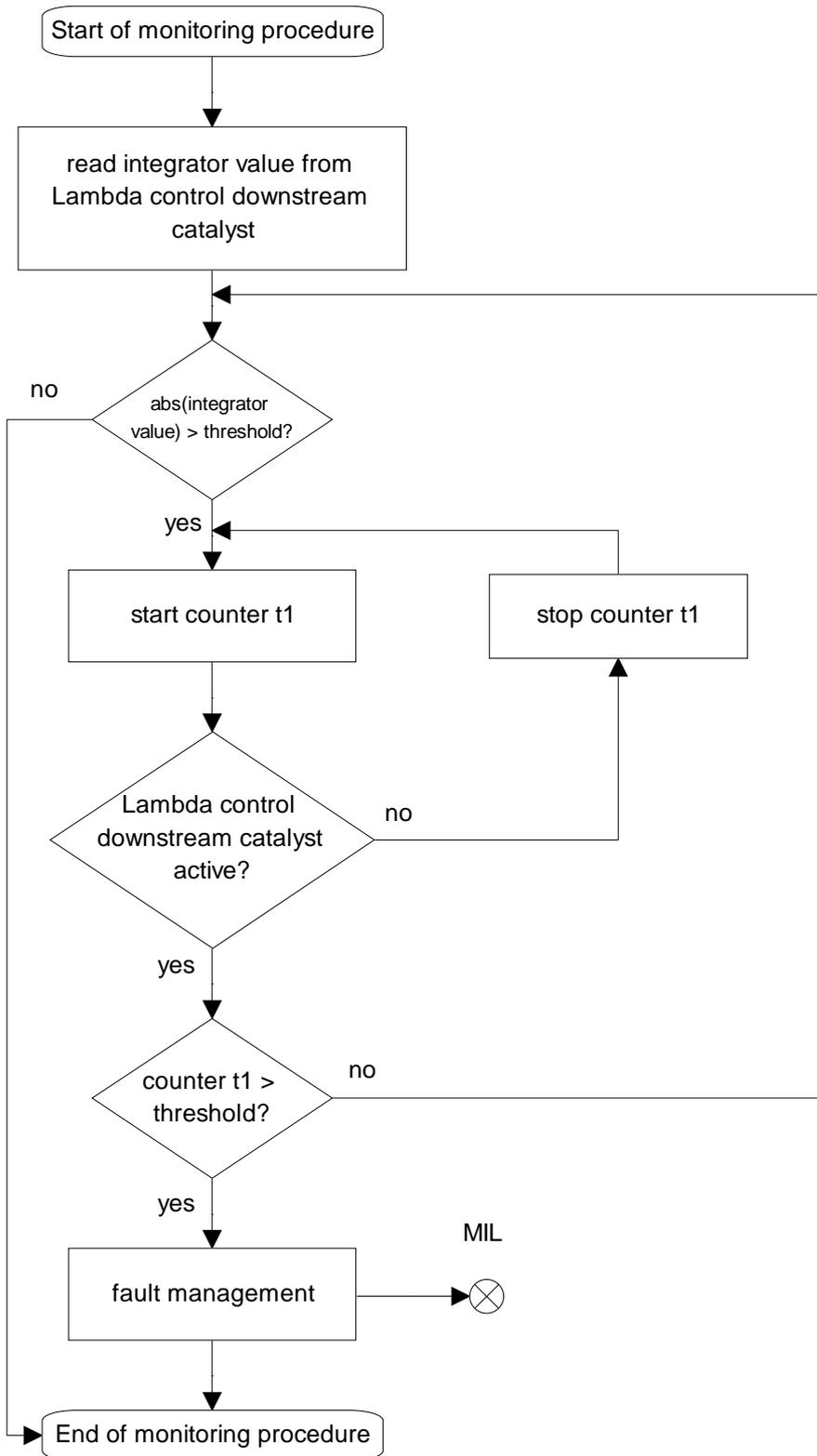
If the adaptive values exceed their plausible ranges, then the MIL is illuminated and the fault is stored.

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Flow chart: Fuel trim



**.07.00.00      OXYGEN SENSOR MONITORING**

**.07.01.00      Calibrations with ASIC CJ 110**

**.07.01.01      General Description**

The Lambda control consists of a linear Oxygen sensor upstream catalyst and a 2-point oxygen sensor downstream catalyst.

**.07.01.02      Monitoring function description**

The sensors are monitored by several single monitoring procedures under the following basic conditions.

- Engine operates in a specific range of speed/load map and
- Modelled catalyst temperature is above a specific value

## **Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

The following checks will be performed on the linear oxygen sensor upstream catalyst:

### Heater Coupling Check (P0130)

This monitoring will detect any short circuits between sensor heater and the Nernst cell of the Oxygen sensor by monitor the Lambda signal. The amplitude signal of Lambda is untypical and changed in the same velocity than heater duty cycle.

### Response Check (P0133)

Any change in the dynamic behaviour of the Oxygen sensor due to ageing, heater fault or contamination will be detected by check of actual amplitude ratio check with stored values.

### Signal activity and rationality checks (P0130)

The Lambda value of oxygen sensor upstream catalyst is compared to the sensor voltage downstream catalyst. Additionally, a check is performed by checking the sensor voltage range. Three diagnostics paths cover the air fuel ratio range of Lambda value (e.g. Lambda=1, lean, rich). A corresponding reaction of sensor voltage downstream catalyst is expected. (See chart)

The following checks will be performed on the oxygen sensor downstream catalyst:

### Oscillation Check (P0139)

The function checks whether the sensor output voltage of oxygen sensor downstream catalyst always remains above or below a specified threshold.

### Fuel cut off Check (P0139)

During coasting, the ECM is monitoring the downstream sensor voltage, which has to go under a specific lean threshold.

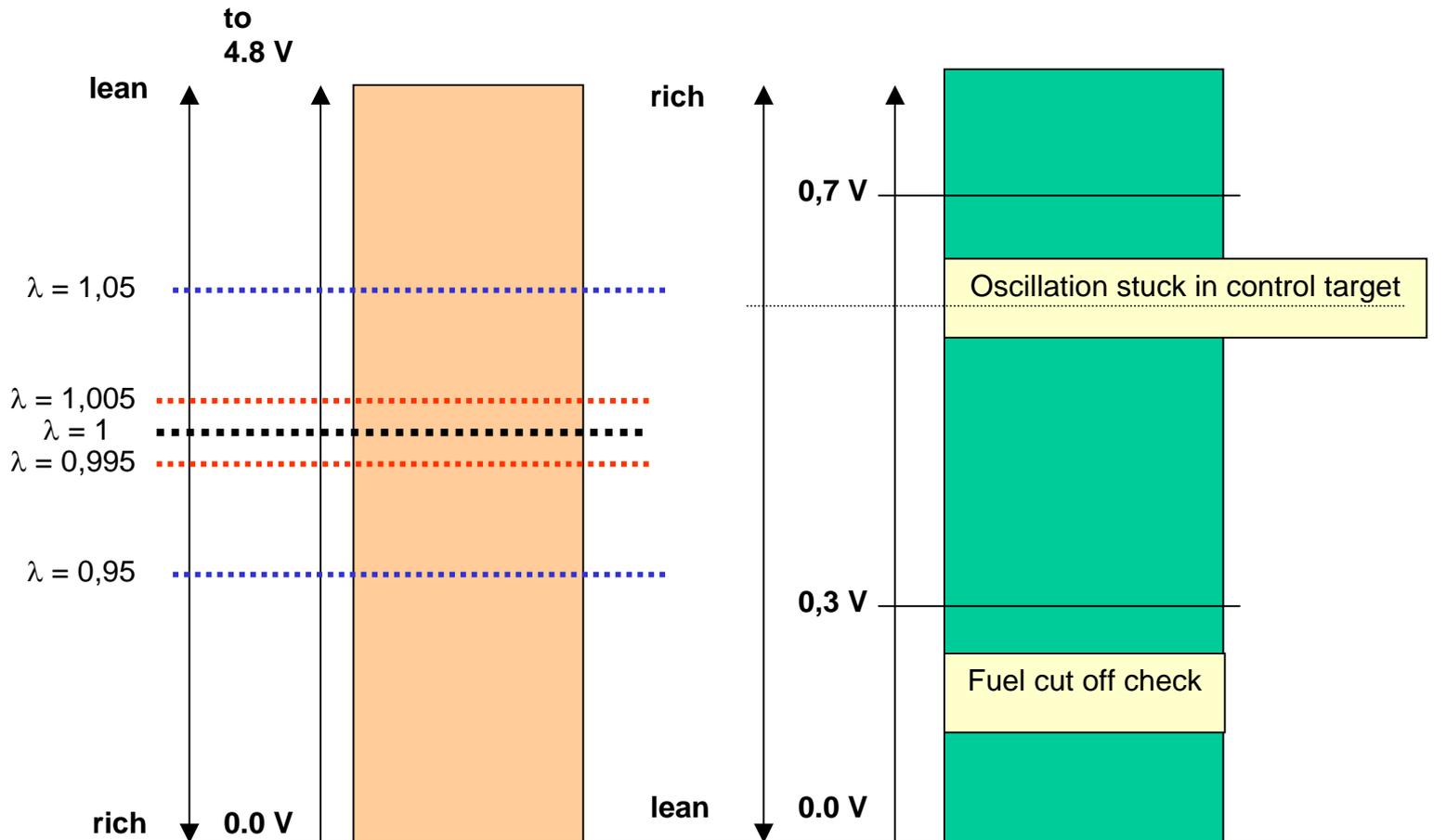
### Output voltage (P0137), Short to battery (P0138) and signal activity check (P0140)

In case the rear O<sub>2</sub> sensor readiness is given a certain sensor signal is expected. If the sensor is bellow or above some signal thresholds, a fault will be stored.

.07.01.03 Chart(s) and flow chart(s)

Front O2 Sensor

Rear O2 Sensor

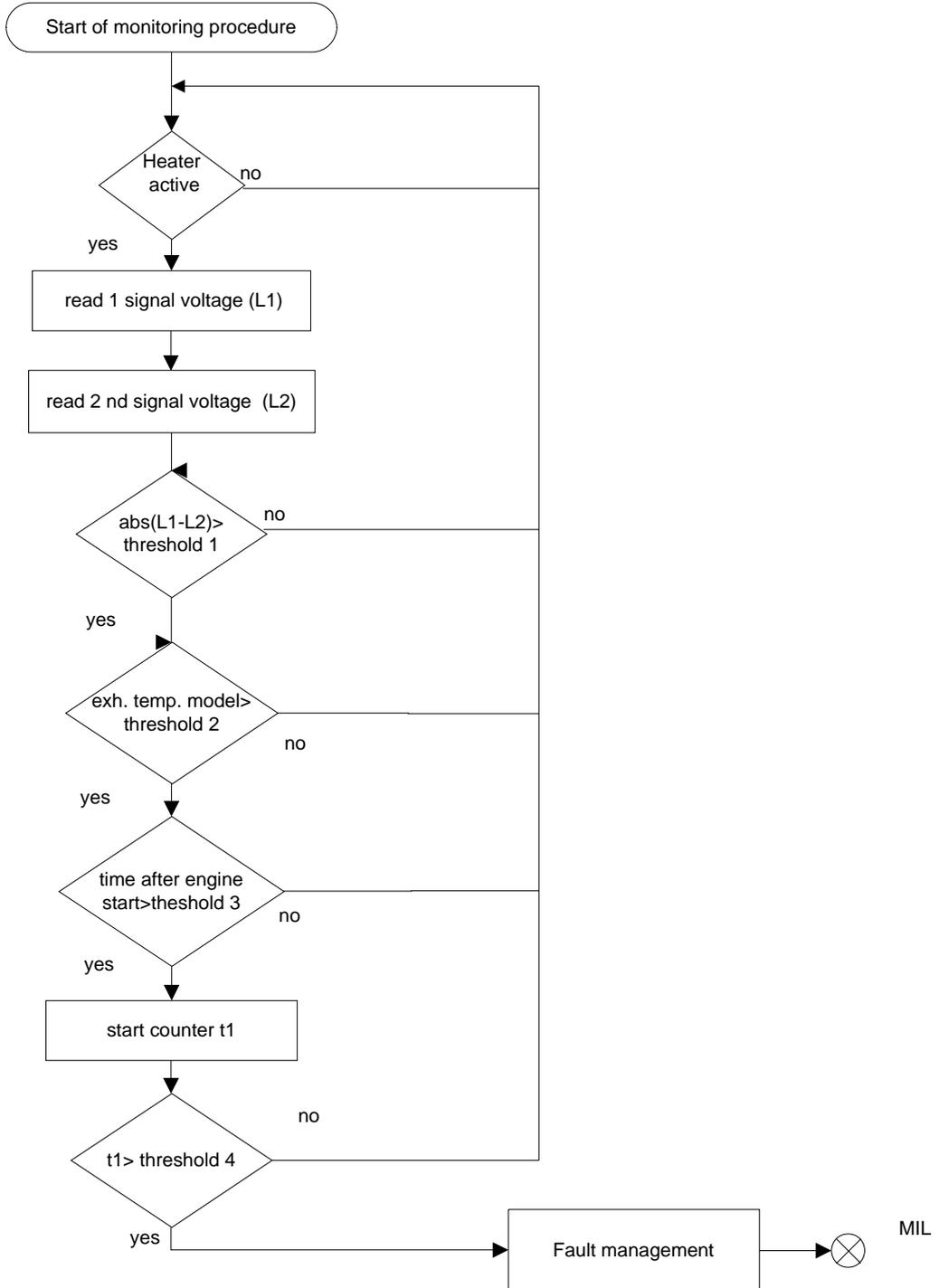


Based on the sensor comparison malfunction will be detected if:

- Front sensor near  $\lambda = 1$  and rear sensor shows  $>0.7V$  or  $< 0,3 V$
- Front sensor lean ( $\lambda > 1.05$ ) and rear sensor rich ( $>0.7V$ )
- Front sensor rich ( $\lambda > 1.05$ ) and rear sensor lean ( $<0.3V$ )
- Rear sensor is not oscillation at reference point (e.g.0.6V)
- During fuel cut off rear sensor signal goes not under threshold (e.g. 0.2V)

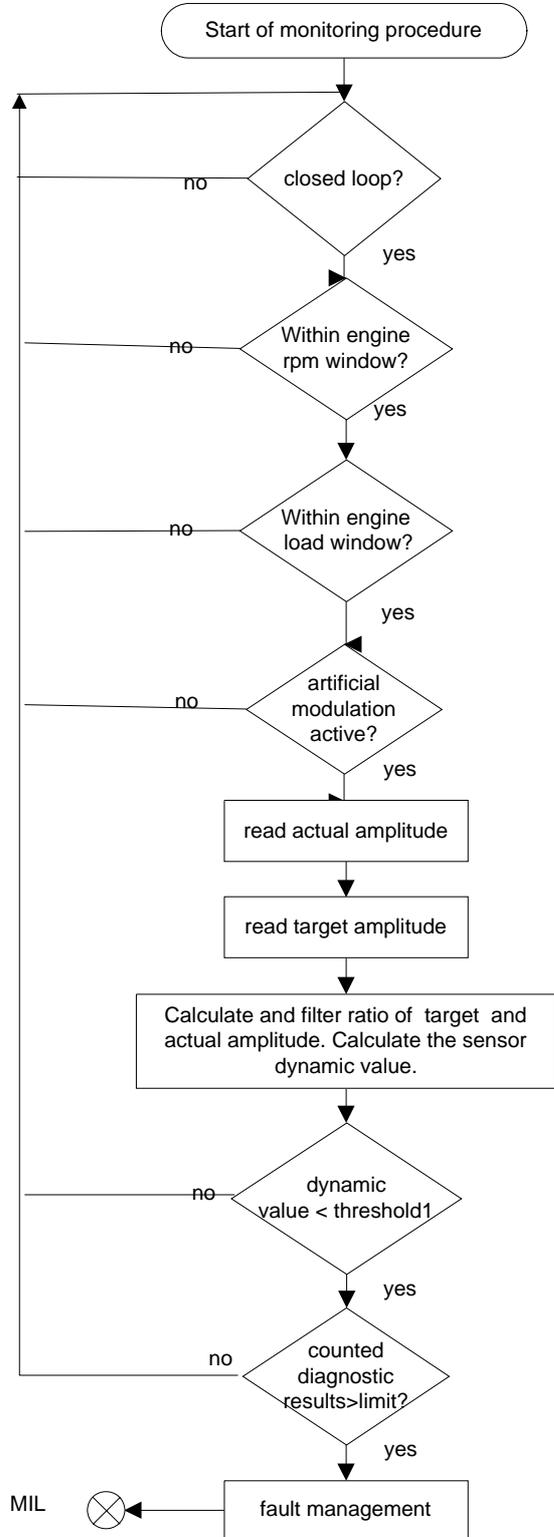
## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Front O2 Sensor Heater Coupling Monitoring	
DTC's	P0130
Threshold 1	Malfunction signal change / msec; typical value: 2 (V/ms)
Threshold 2 / 3	Typical value: 200 °C / 25sec
Threshold 4	Monitor time length: 30 amplitudes



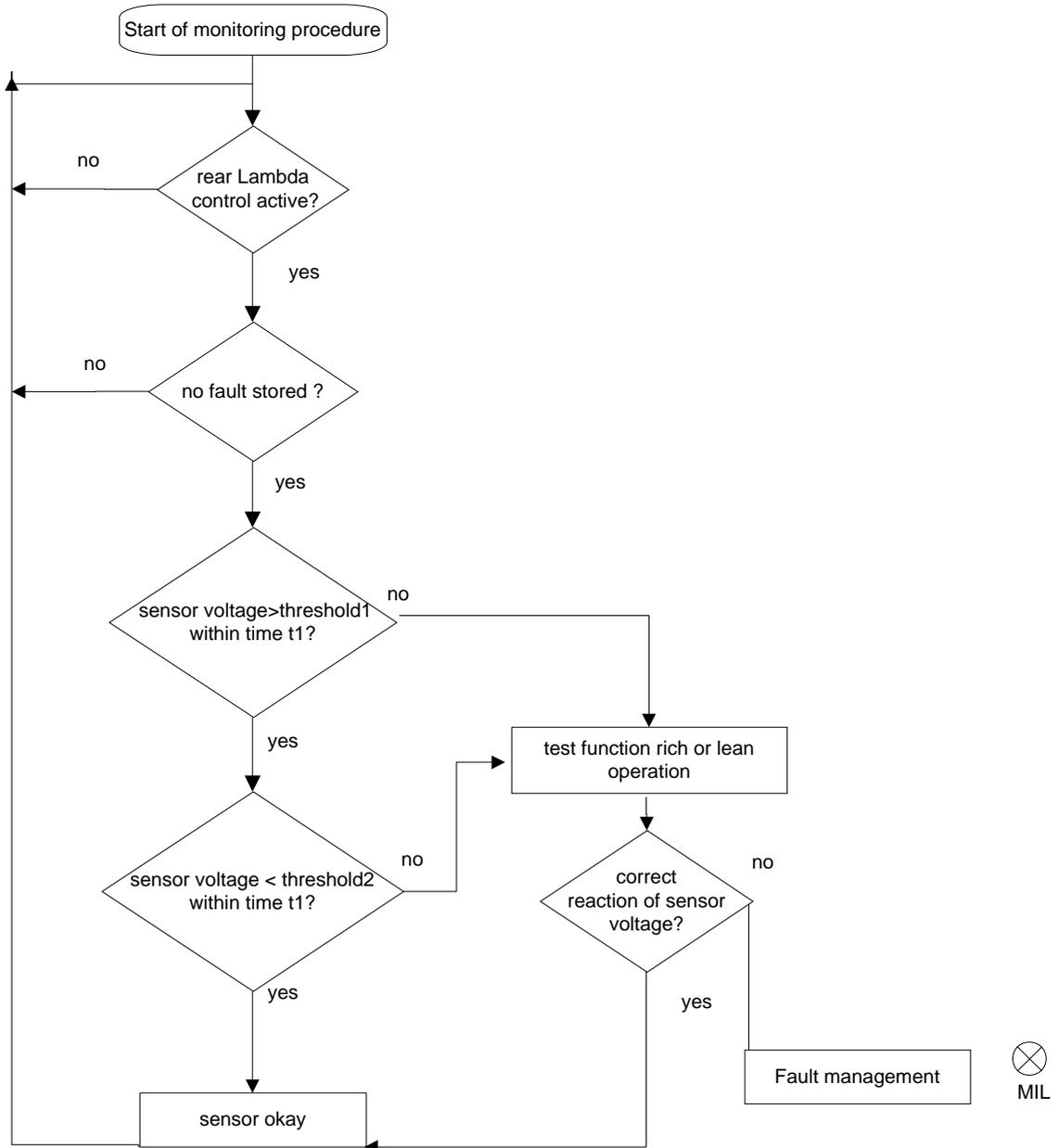
# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Front O2 Sensor Response Check	
DTC's	P0133
Threshold 1	Malfunction criteria
Limit	Monitor time length 30 amplitudes



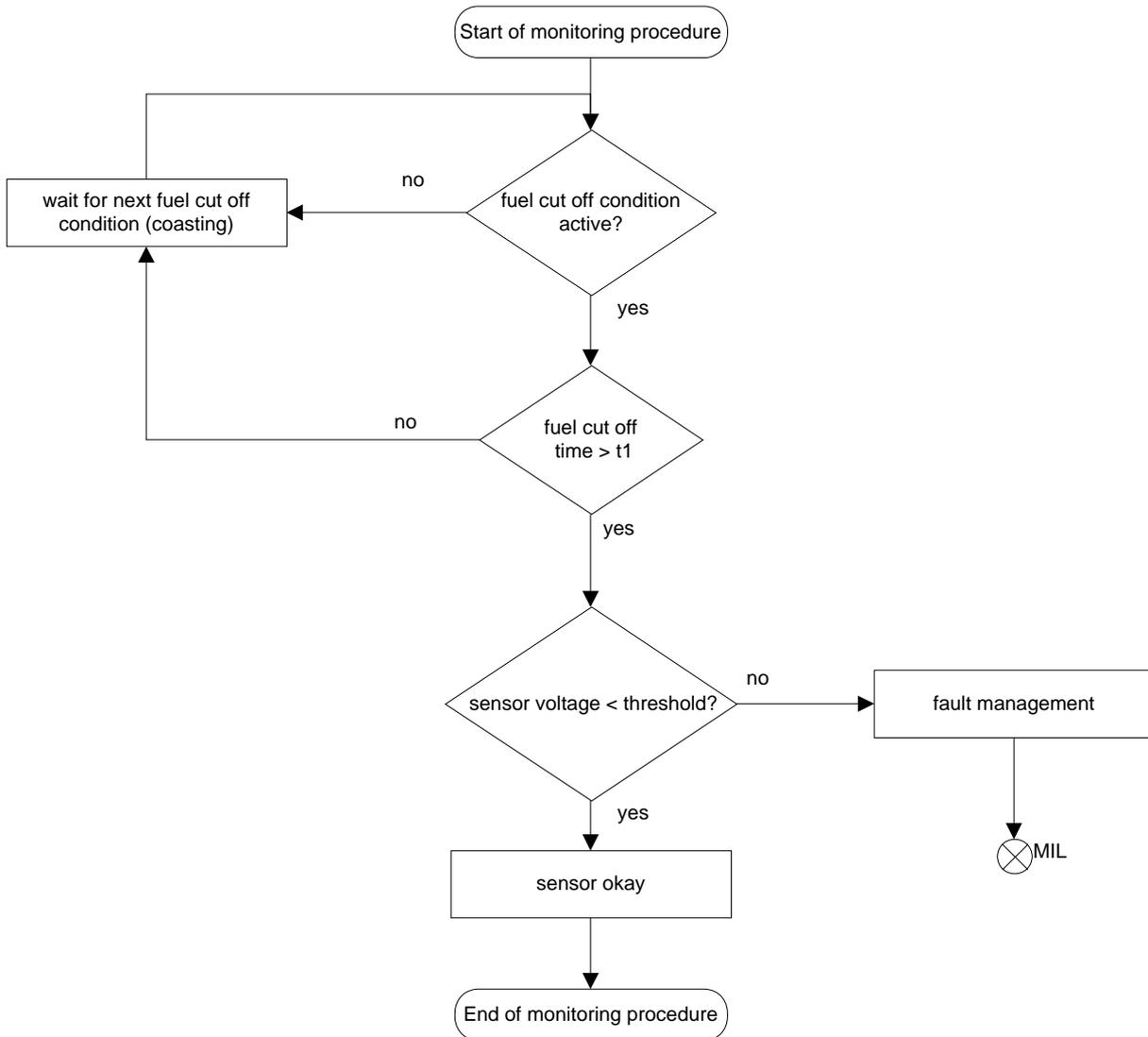
## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Rear O2 Sensor Oscillation check	
DTC's	P0139
Threshold 1 and 2	Malfunction Criteria; typical values: 0.58 .. 0.6V
Limit	Monitor time length 30 amplitudes



## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Rear O2 Sensor Fuel Cut Off Check	
DTC's	P0139
Time t1	Duration of fuel cut off phase; Typical value 5s
Threshold	Malfunction criteria; typical value: < 0.2V



**.07.02.00 Oxygen Sensor Heater Monitoring**  
**.07.03.01 General description (ASIC CJ 110)**

For proper function of the Lambda sensor, the sensor element must be heated.

**.07.02.02 Monitor function description**

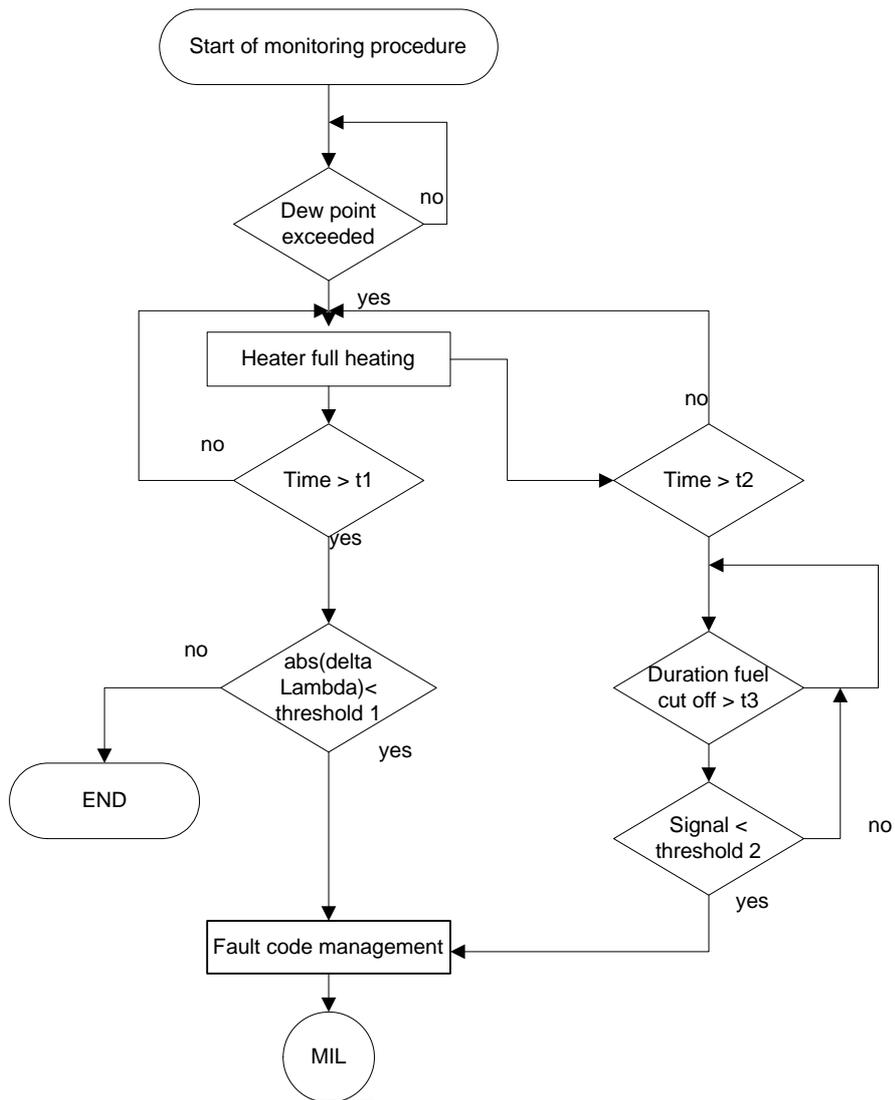
**Linear Oxygen sensor upstream catalyst** Any fault in regard to sensor heater will either result in a lost or in a delay of sensor readiness. The diagnosis measures the time between the heater is switched on and the oxygen sensor readiness. The sensor readiness is indicated by a corresponding sensor voltage variation.

**Oxygen sensor downstream catalyst (2 point sensor)**

For diagnostic of the sensor heater a specific current pulse is supplied via a load resistance and the voltage is measured. The internal resistance of the sensor heater is calculated with the voltage deviation. The result will be compared with a reference map resistance, which considers ageing and sampling deviations. In case of internal resistance > map resistance the diagnosis stores a fault and the MIL will be illuminated.

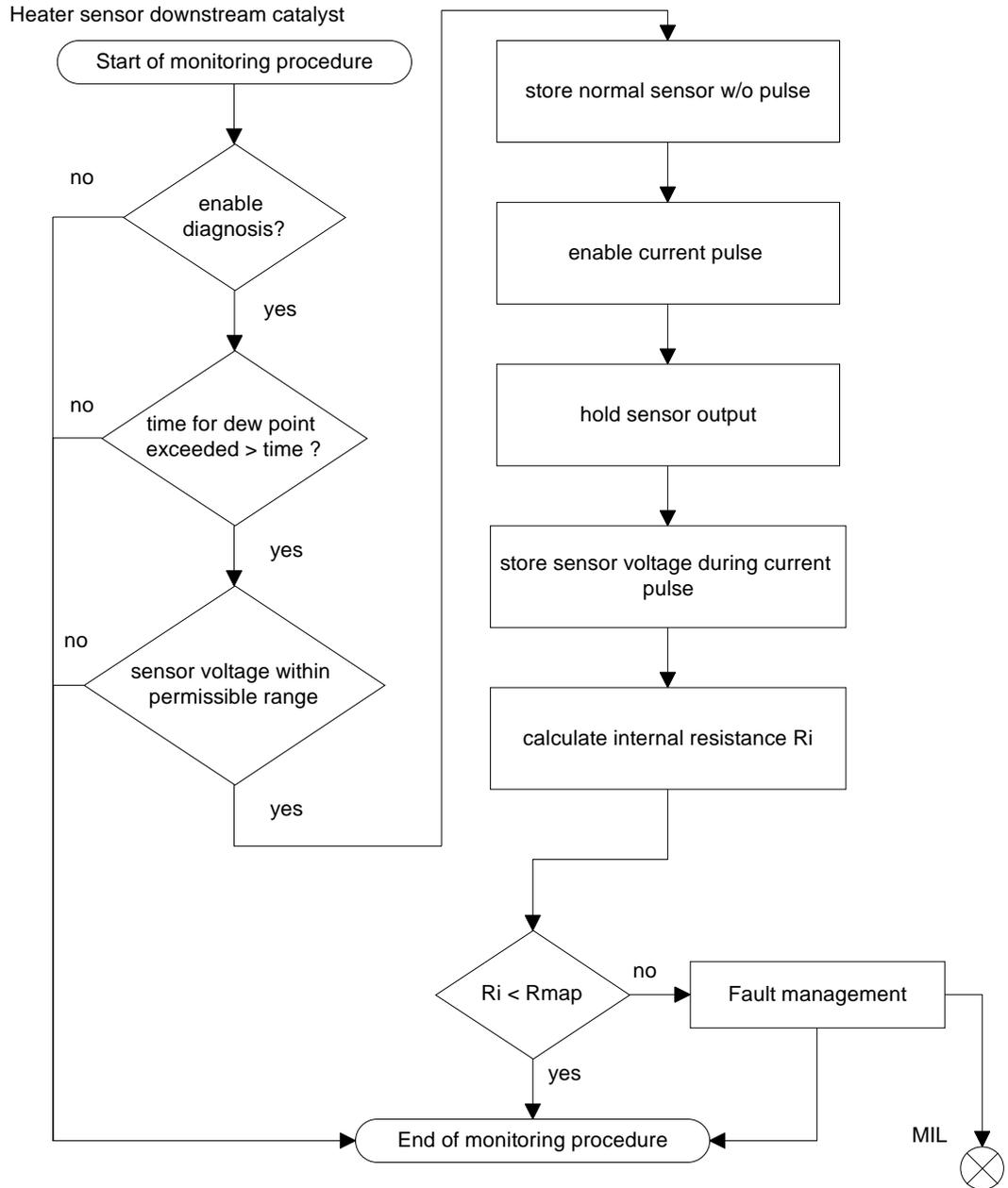
07.02.03 Chart(s) and Flow Chart(s)

Oxygen Sensor Heater Upstream Catalyst	
DTC's	P0135
Time t1 / t2	Duration full heating; typical value 25s / 70s
Time t3	Duration fuel cut off; typical value 3 s
Threshold 1	Malfunction criteria; delta lambda
Threshold 2	Malfunction criteria; sensor voltage



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Oxygen Sensor Heater downstream Catalyst	
DTC's	P0141
Enable criteria	Modelled exhaust temperature, IAT
Ri < Rmap	Comparison of actual and calculated resistance



**.07.03.00 Calibrations with ASIC CJ 125/120**

**.07.03.01 General Description**

The Lambda control consists of a linear Oxygen sensor upstream catalyst and a 2-point oxygen sensor downstream catalyst.

**.07.03.02 Monitor function description**

The following checks will be performed on the linear oxygen sensor upstream catalyst:

Rationality Check

Any deviation from the characteristic curve of oxygen sensor upstream catalyst due to poison, ceramic cracks, characteristic shift down (CSD) or a leakage between both Oxygen sensors will be detected by the control loop downstream catalyst and by comparison of the sensor signals.

The integrator value of the second control loop detects small shifts of the sensor characteristic to lean or to rich. The signal comparison during steady state conditions quickly detects major deviations in sensor characteristics caused by serious faults (e.g. ceramic cracks).

For the fault decision the downstream Oxygen sensor has to be checked too (Oscillation and/or fuel cut-off check).

Heater Coupling Check

This monitoring function will detect any short circuits between sensor heater and the Nernst cell of the Oxygen sensor by watching the Lambda signal. The ECM checks the Lambda value variation. The heater is operated by a pulsating signal with a frequency of two Hertz. The sensor signal characteristic is checked for noises with a significant level and a frequency of the heater operation. If the level of noises is greater than a threshold, a low resistance short cut between heater and pump current or the current of the Nernst cell is detected.

Dynamic Check

Any change in the dynamic behaviour of the Oxygen sensor due to ageing, heater fault or contamination will be detected by check of actual amplitude ratio check with stored values.

Wire and IC-Check

The hardware of the Oxygen sensor consists of an IC (CJ 125) with the capability of self-diagnostics. The self-diagnostic functions of the IC detects communication faults between ECM and the sensor, insufficient voltage supply, shorts in the sensor lines to ground and to battery.

Open wire on the four sensor lines, adjustment line (IA), virtual mass line (VM), pump current line (IP) and Nernst voltage (UN) will be detected by a system plausibility check. The evaluations of the system plausibility is based on sensor voltage, internal resistance, target Lambda, actual Lambda and the reaction of the controller.

The following checks will be performed on the oxygen sensor downstream catalyst:

## **Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

### Oscillation Check

The function checks whether the sensor output voltage of the oxygen sensor downstream catalyst always remains above or below a specified threshold.

### Fuel cut off Check

During coasting, the ECM is monitoring the downstream sensor voltage, which has to go below a specific lean threshold. The diagnostic is enabled if coasting was detected for a specific time.

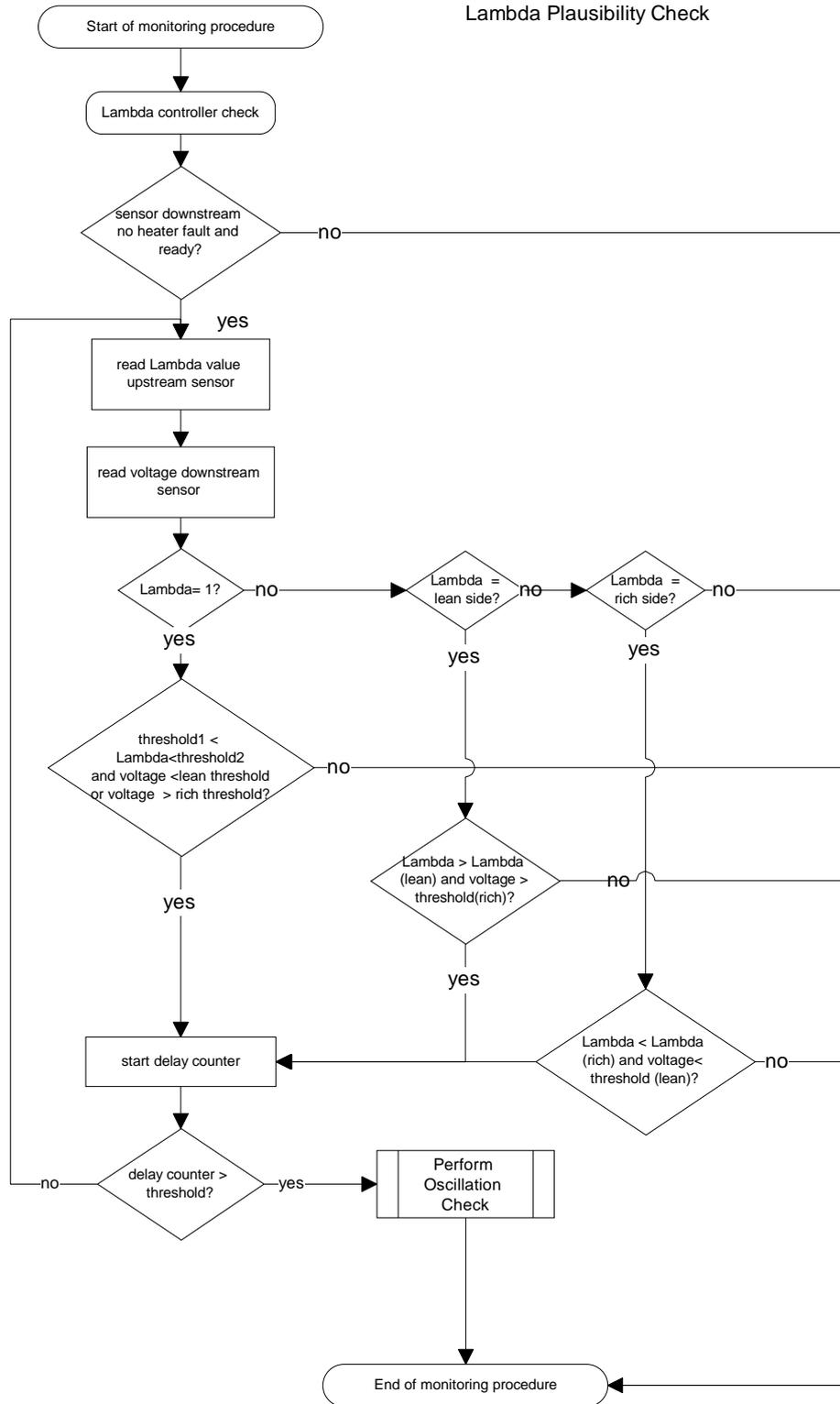
### Signal check, short to battery check and signal activity check

In case the rear O<sub>2</sub> sensor readiness is given a certain signal voltage is expected. If the sensor is below or above some signal thresholds, a fault will be stored.

.07.03.03

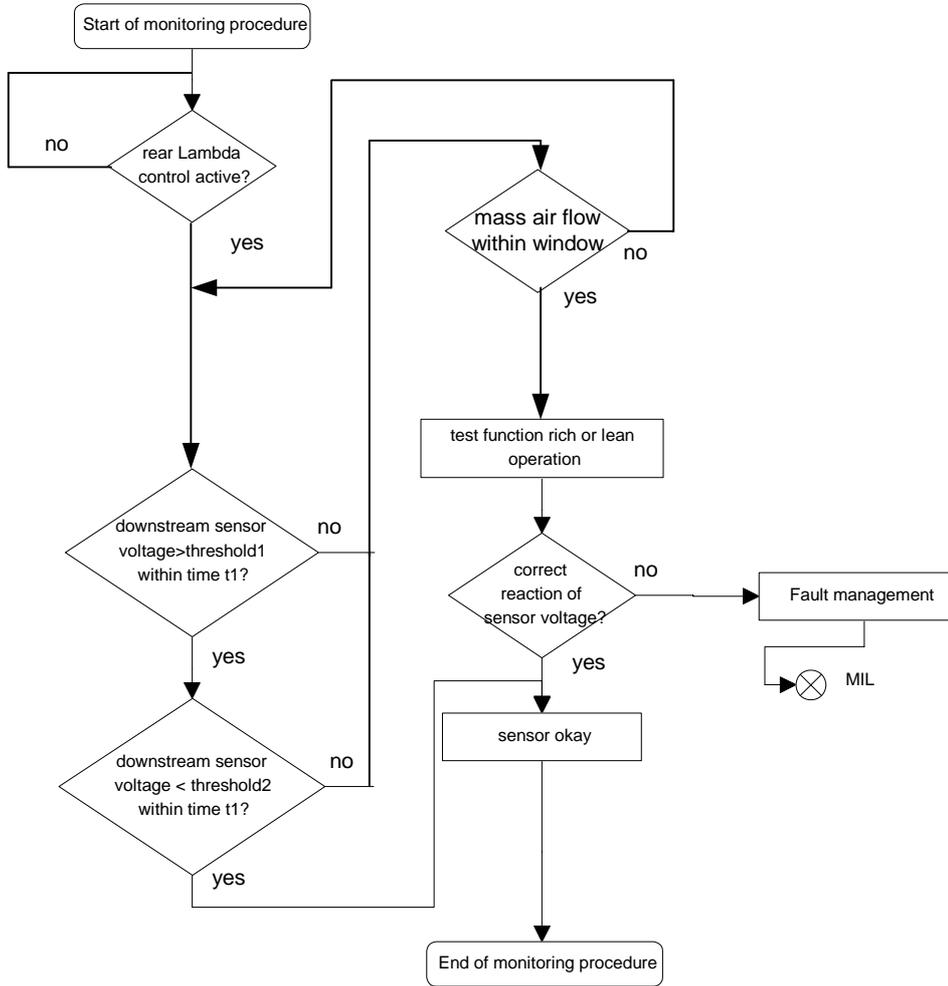
Chart(s) and Flow Chart(s)

Flow chart: Rationality Monitoring (Oxygen Sensor Upstream Catalyst)



**Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

**Flow chart: Oscillation Monitoring (Oxygen Sensor Downstream Catalyst)**



**Flow Chart: Fuel Cut-Off Monitoring (Oxygen Sensors Downstream Catalysts)**

See other calibrations.

**.07.04.00 Oxygen Sensor Heater Monitoring (ASIC CJ 125/120)**  
**.07.04.01 General description**

For proper function of the Oxygen sensors, the sensor element must be heated up. The heating up is controlled by the heater control.

**.07.04.02 Monitor function description**

**Linear Oxygen sensor upstream catalyst**

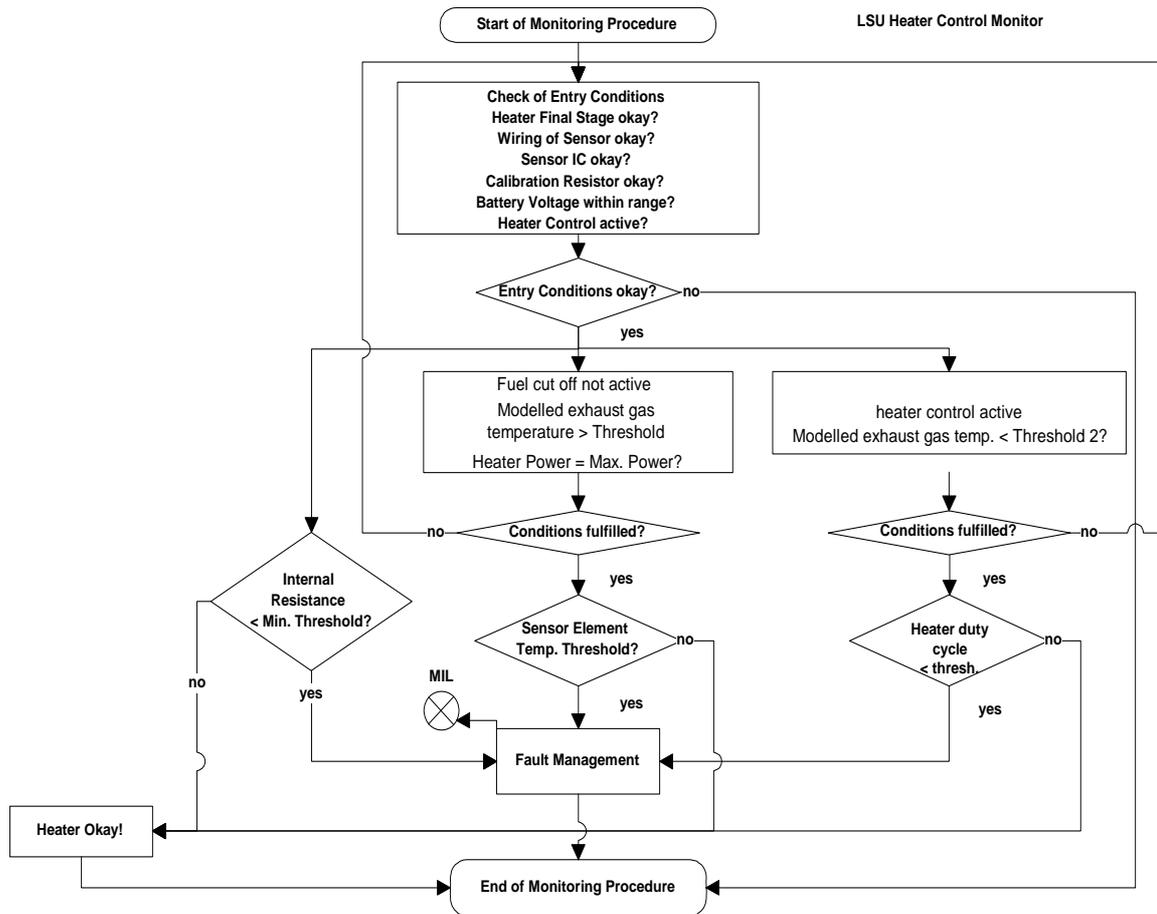
Any fault in regard to sensor heater will either result in a lost or in a delay of sensor readiness.

**Oxygen sensor downstream catalyst (2 point sensor)**

For diagnostic of the sensor heater a specific current pulse is supplied via a load resistance and the voltage is measured. The internal resistance of the sensor heater is calculated with the voltage deviation. The result will be compared with a reference resistance map, which considers ageing and sampling deviations. In case of internal resistance > map resistance the diagnosis stores a fault and the MIL will be illuminated.

**.07.04.03 Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy Chart(s) and Flow Chart(s)**

Flow Chart: Oxygen Sensor Heater Control Upstream Catalyst



Flow Chart: Oxygen Sensors downstream catalyst

See other calibrations

### **.07.05.00** ..... **SULEV applications**

#### **.07.05.01** ..... **General description**

The Lambda control consists of a linear Oxygen sensor (LSU) upstream catalyst and two Oxygen sensors (LSF1 and LSF2) downstream front catalyst and post main catalyst. The control loops downstream catalysts correct deviations of the upstream oxygen sensor (LSU).

All three sensors are monitored by several single monitoring procedures under the following basic conditions.

#### **.07.05.02** ..... **Monitor function description**

The following checks will be performed on the linear oxygen sensor (LSU) upstream catalyst:

##### Plausibility Check

Any deviation from the characteristic curve of oxygen sensor upstream catalyst due to poison, ceramic cracks, characteristic shift down (CSD) or a leakage between both Oxygen sensors (LSU and LSF 1) will be detected by the control loop downstream catalyst and by comparison of the sensor signals.

The integrator value of the second control loop detects small shifts of the sensor characteristic to lean or to rich. The signal comparison during steady state conditions quickly detects major deviations in sensor characteristics caused by serious faults (e.g. ceramic cracks).

For the fault decision the Oxygen sensor downstream the first portion of the catalyst has to be checked too (Oscillation and/or fuel cut-off check).

##### Heater Coupling Check

This monitoring function will detect any short circuits between sensor heater and the Nernst cell of the Oxygen sensor by watching the Lambda signal. The ECM checks the Lambda value variation. The heater is operated by a pulsating signal with a frequency of two Hertz. The sensor signal characteristic is checked for noises with a significant level and a frequency of the heater operation. If the level of noises is greater than a threshold, a low resistance short cut between heater and pump current or the current of the Nernst cell is detected.

##### Dynamic Check

Any change in the dynamic behavior of the Oxygen sensor due to aging, heater fault or contamination will be detected by watching the slope of the Lambda value during the switch from lean to rich fuel mixture (natural frequency control of fuel mixture active). If the slope of the sensor signal exceeds a specific value the monitoring function is calculating the ratio of actual Lambda slope versus target Lambda slope. If a specific numbers of those slope ratios are less than a threshold, a fault is detected.

##### Check for Sensor at ambient air (out of exhaust system)

Under the condition of active injection valves and a Lambda value of  $< 1.6$ , a voltage significant less than 4.2 V is expected at the self-diagnostic IC of the LSU.

##### Wire and IC-Check

## **Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

The hardware of the Oxygen sensor consists of an IC (CJ 125) with the capability of self-diagnostics. The self-diagnostic functions of the IC detects communication faults between ECM and the sensor, insufficient voltage supply, shorts in the sensor lines to ground and to battery.

Open wire on the four sensor lines, adjustment line (IA), virtual mass line (VM), pump current line (IP) and Nernst voltage (UN) will be detected by a system plausibility check. The evaluations of the system plausibility is based on sensor voltage, internal resistance, target Lambda, actual Lambda and the reaction of the controller.

The following checks will be performed on the oxygen sensors (LSF1 and LSF2) downstream catalyst:

### Oscillation Check

The function checks whether the sensor output voltage of oxygen sensors (LSF 1 and LSF2) downstream catalyst always remains above or below a specified threshold.

The second control loop is designed as a natural frequency control and based on the Oxygen sensor (LSF1) post front catalyst. The voltage of the LSF1 triggers the change of fuel mixture. If the trigger point is not crossed although the control loop is closed, a timer is started. In case of no signal change within a specific time, ECM enforces a specific mixture change while watching Oxygen sensor (LSF1) voltage.

In case of Oxygen sensor (LSF1) signal shows permanently "lean" voltage, ECM is forcing an enrichment of mixture. If sensor voltage shows still lean, a "stuck low" fault is detected.

In case of Oxygen sensor (LSF1) signal shows permanently "rich" voltage, ECM enables lean out of mixture. If sensor voltage shows still rich, ECM is watching the sensor signal during the next coasting condition. In case of no signal change during coasting, a "stuck high" fault is detected.

The third control loop is designed as commanded control and based on the Oxygen sensor (LSF2) post main catalyst. The controller maintains an optimal constant voltage of the third control loop. The target voltage depends on the operating point and is taken from a map. During active control, the target voltage switches between rich and lean. In case of no reaction of the Oxygen sensor (LSF2) output according the commanded control, ECM is forcing the same enrichment/ lean out of fuel mixture in order to monitor the sensor output voltage.

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Fuel cut off Check

During coasting, the ECM is watching the downstream sensor voltage, which has to go under a specific lean threshold. The diagnostic is enabled if coasting was detected for a specific time and the integrated air mass exceeds a specific threshold.

### Offset monitoring Oxygen sensor (LSF1) downstream first portion of the catalyst

If the integral portion of the third control loop is exceeding a specific threshold while commanded control is active, an offset fault for the Oxygen sensor post front catalyst is detected.

Monitoring of electrical errors of sensor upstream and downstream catalyst

### Implausible voltages

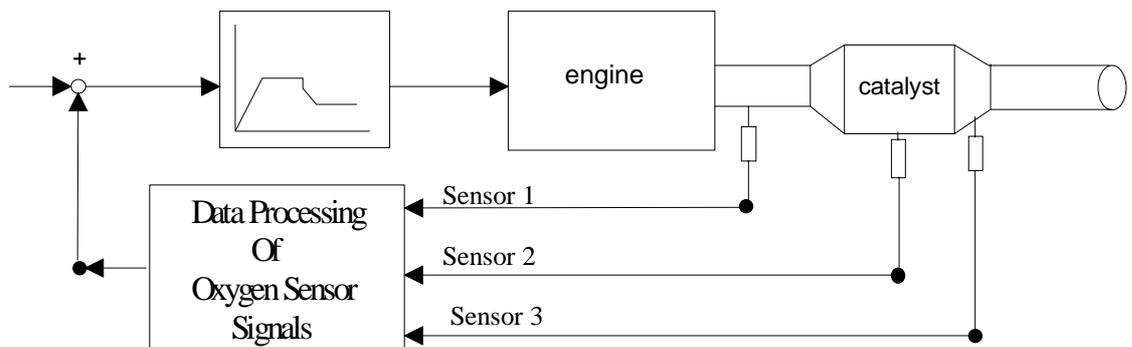
ADC-voltages exceeding the maximum threshold VMAX are caused by a short circuit to UBatt.

ADC-voltages falling below the minimum threshold VMIN are caused by a short circuit of sensor signal or sensor ground to ECM ground.

An open circuit of the sensors (upstream and downstream catalyst) can be detected, if the ADC-Voltage is remaining in a specified range after the sensor has been heated.

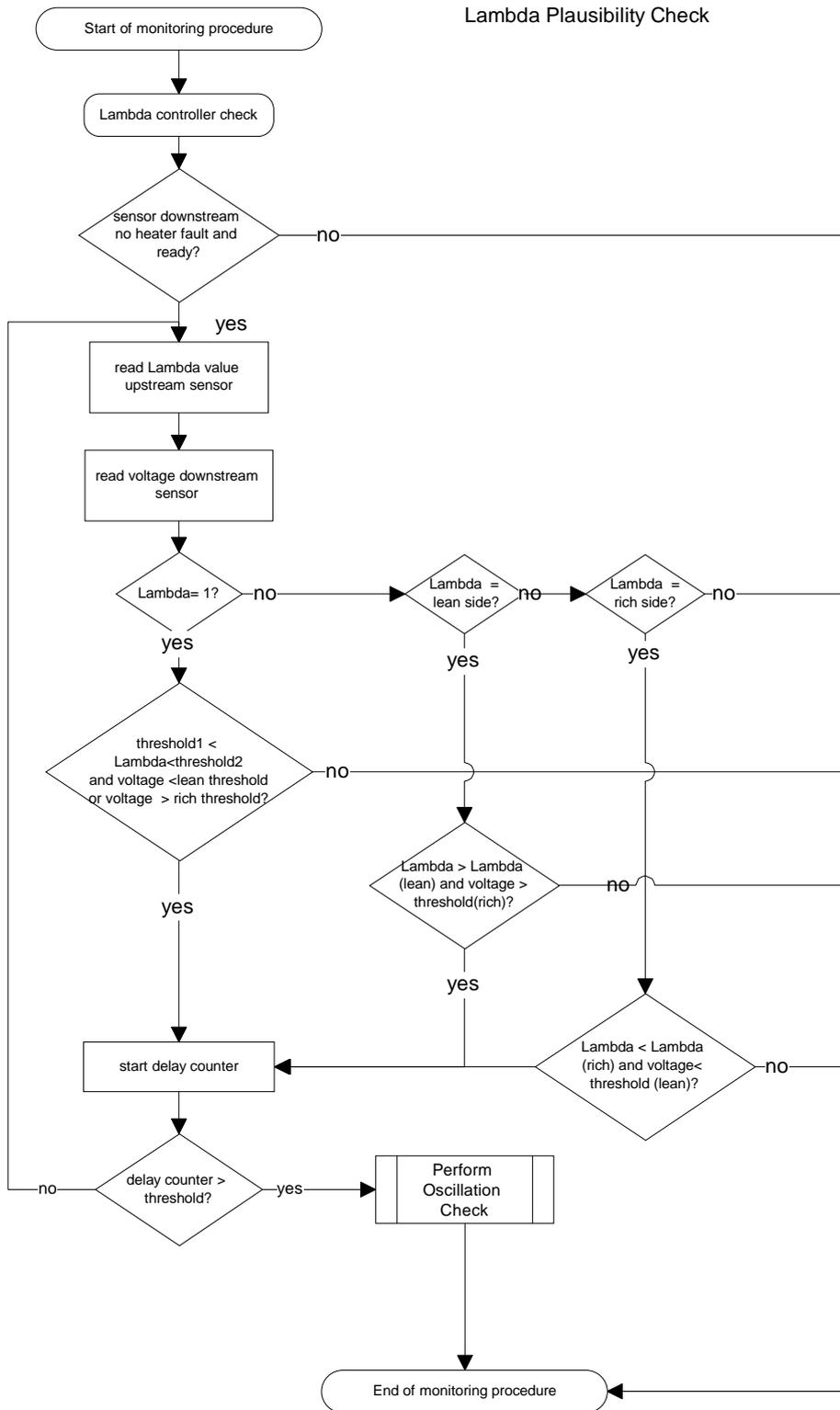
.07.05.03

### Chart(s) and flow chart(s)



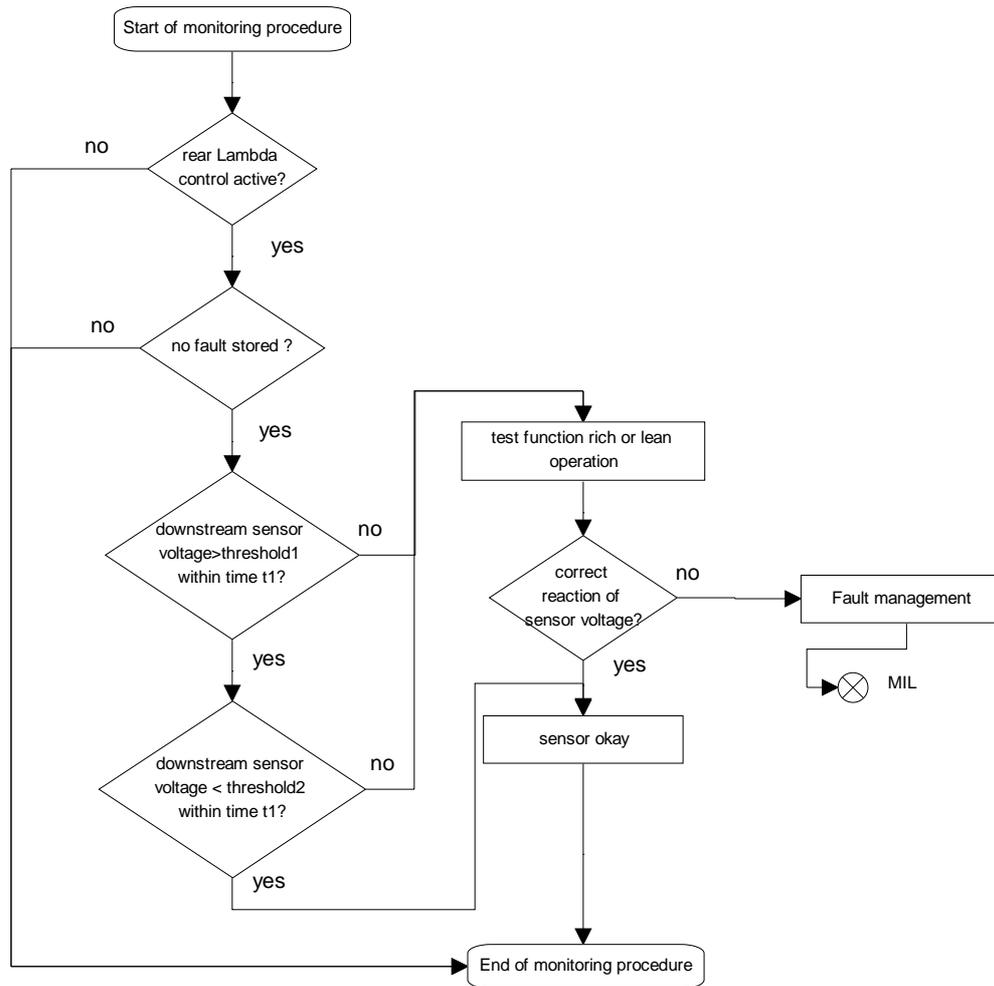
# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Flow chart: Plausibility Monitoring (LSU O2 Sensor Upstream Catalyst) SULEV applications



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

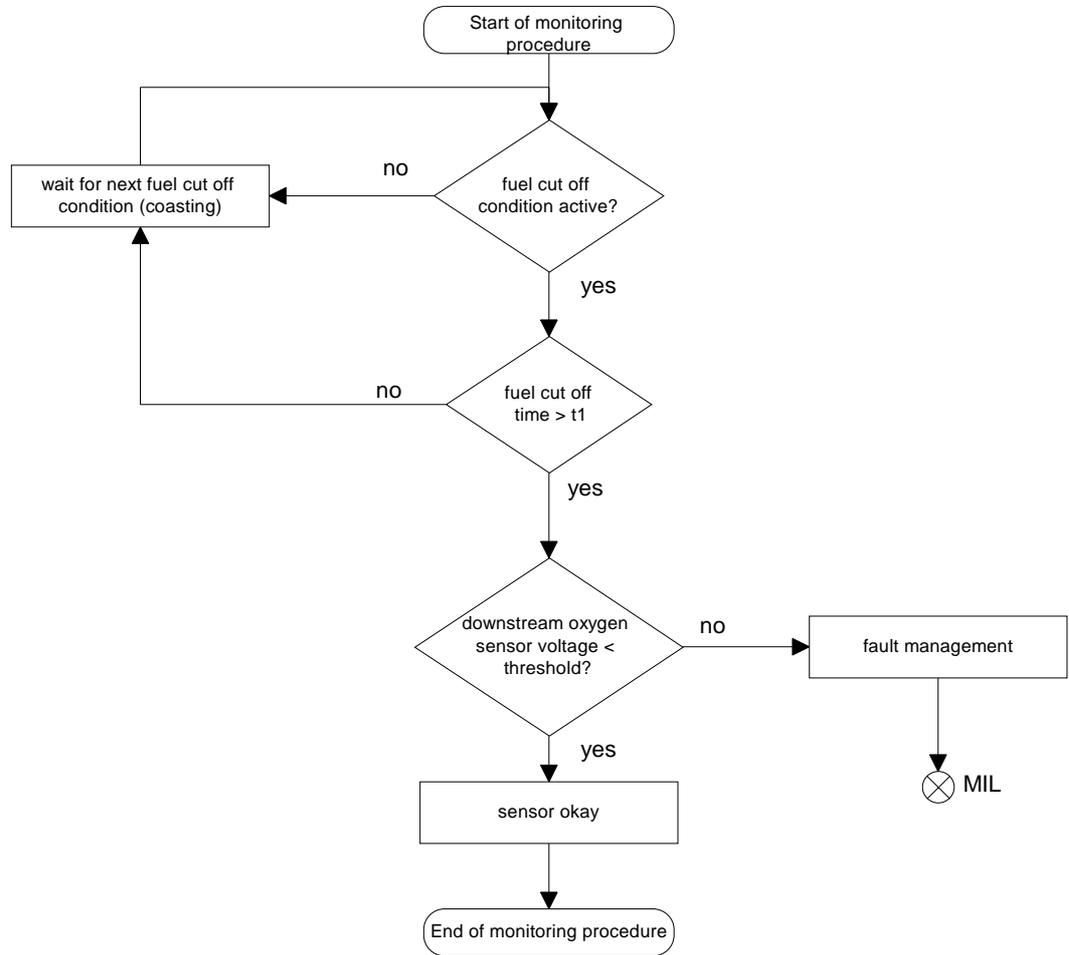
Flow chart: Oscillation Monitoring (LSF1/2 O2 Sensor Downstream Catalyst)



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

## Fuel Cut-Off Monitoring (LSF1/LSF2, Oxygen Sensors Downstream Catalysts)

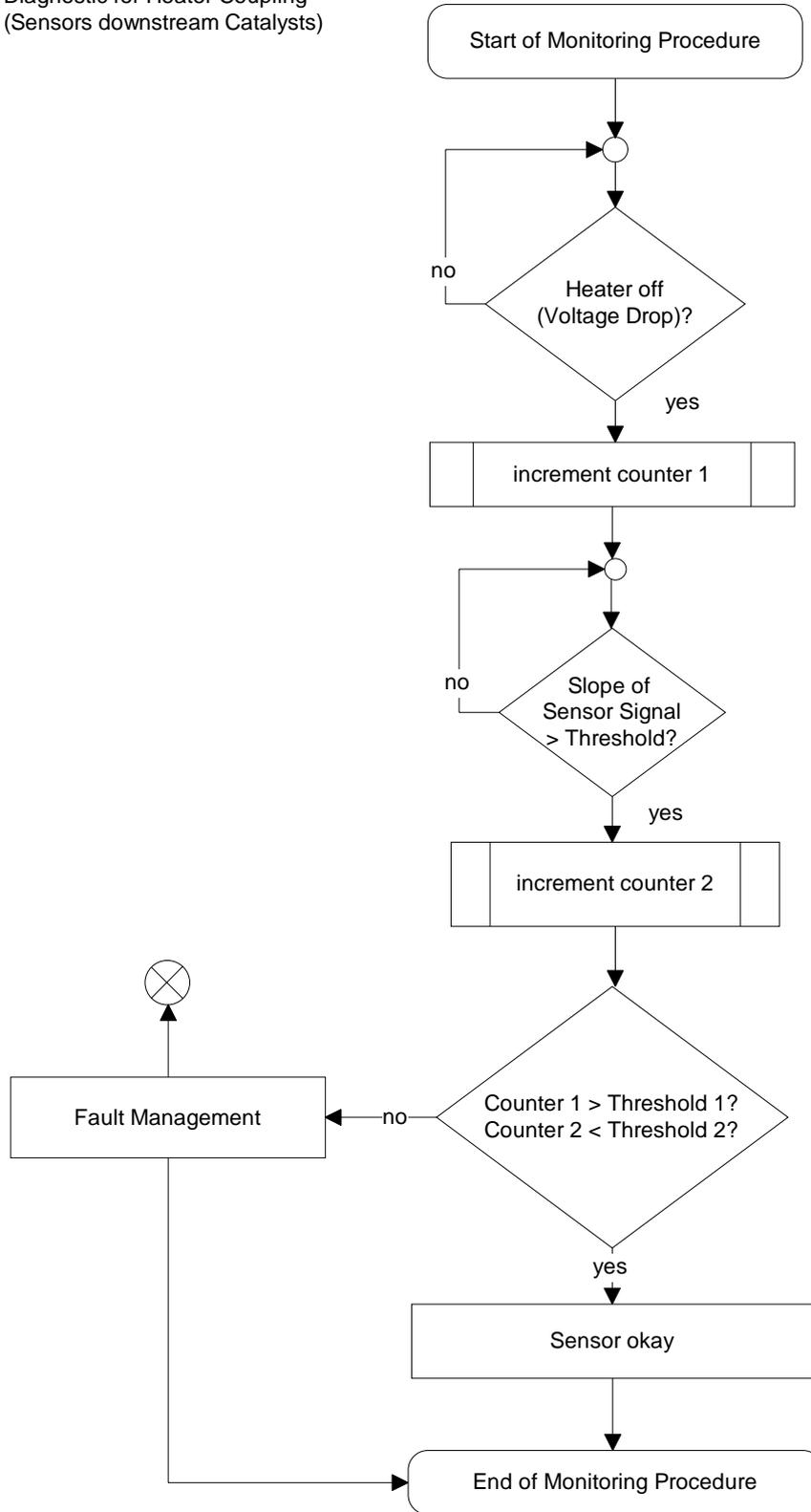
Fuel cut-off check



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

## Oxygen Sensors Monitor Heater Coupling (LSF1 / LSF2)

Diagnostic for Heater Coupling  
(Sensors downstream Catalysts)



**.07.06.00 Oxygen Sensor Heater Monitoring (SULEV)**  
**.07.06.01 General description**

For proper function of the Oxygen sensors, their ceramic elements must be heated. A non-functioning heater delays or prevents either the sensor readiness (LSU) or the proper signal output (LSF1/LSF2) for closed loop control and thus influences emissions.

**Oxygen sensor upstream catalyst (LSU)**

The heater control loop is integrated within the oxygen sensor hardware and has to achieve a target temperature of about 750 °C of the ceramic element.

**Oxygen sensors downstream catalysts (LSF1 and LSF2)**

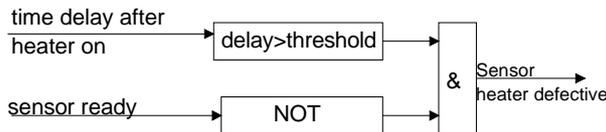
For diagnostic of the sensor heater a specific current pulse is supplied via a load resistance and the voltage is measured. The intern resistance of the sensor heater is calculated with the voltage deviation. The result will be compared with a reference map resistance, which considers aging and sampling deviations. In case of internal resistance > map resistance the diagnosis stores a fault and the MIL will be illuminated.

**.07.06.02 Monitor function description)**

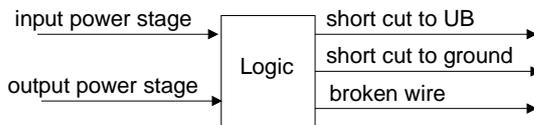
**Monitoring Structure (Oxygen sensor upstream catalyst)**

Heater Monitoring of Linear Oxygen Sensor Upstream Catalyst

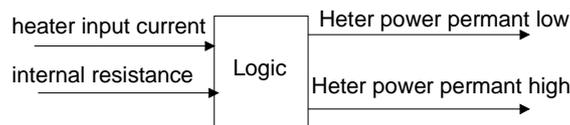
Operating readiness



Power stage (final stage)



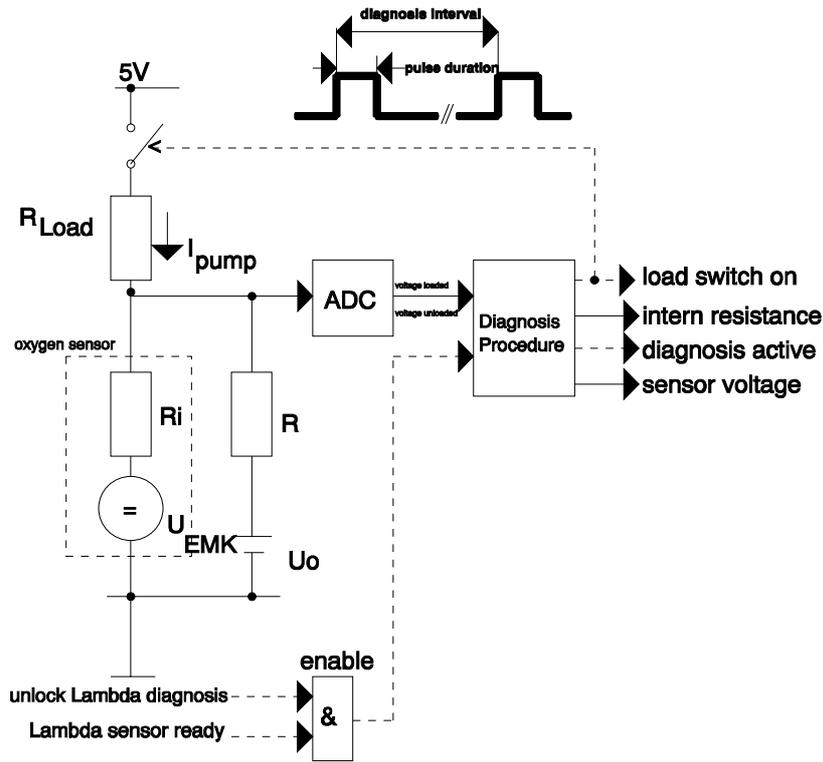
Heater Control Loop



Characteristics: - Switch on of sensor heater is ECM controlled

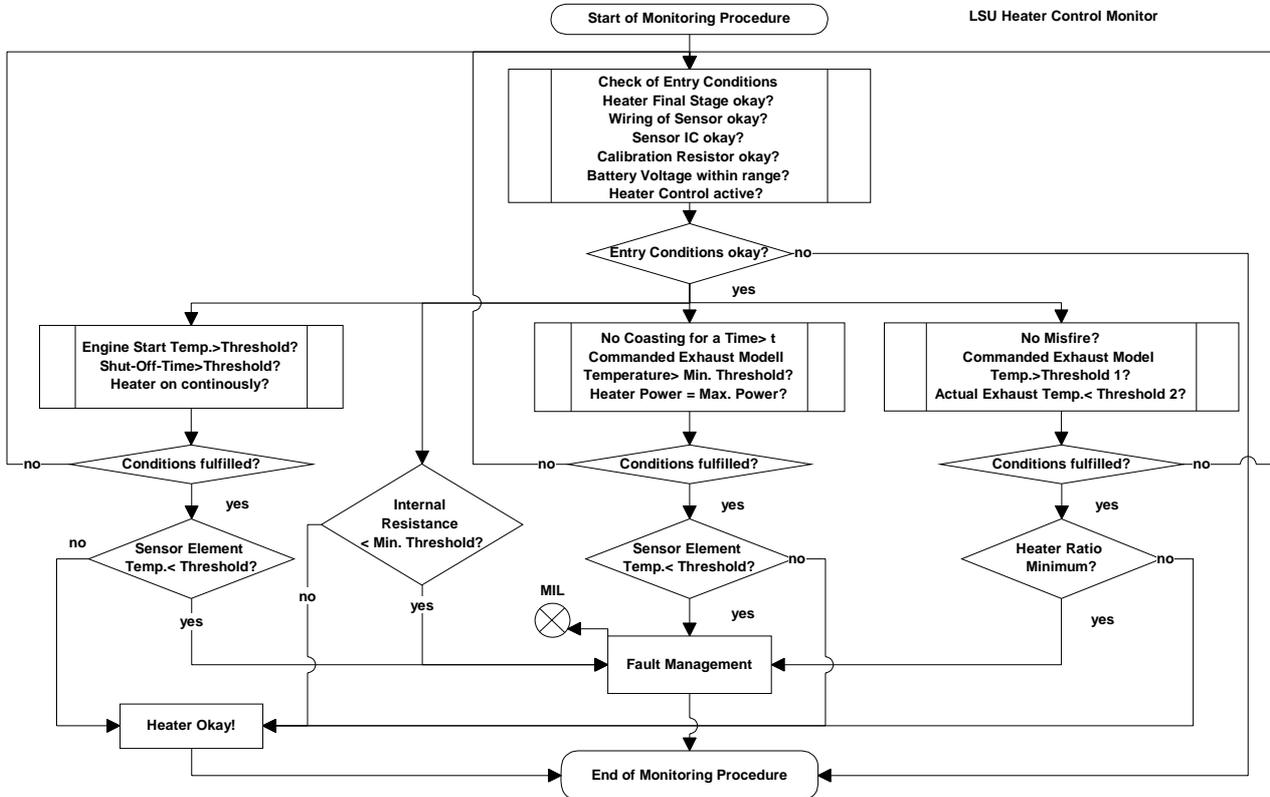
# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

## Monitoring Structure (Oxygen Sensor Downstream Catalyst)



.07.06.03 Chart(s) and Flow Chart(s)

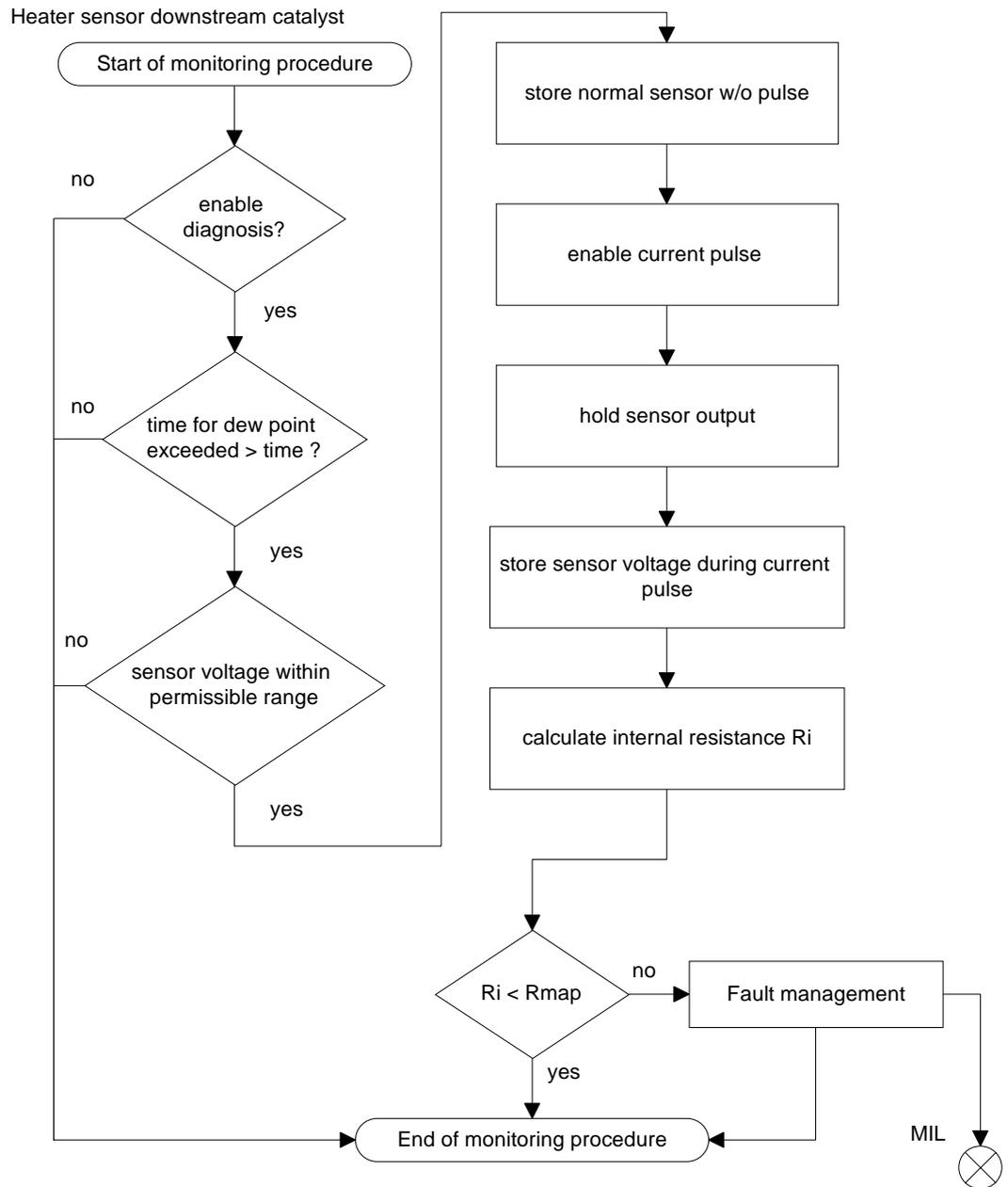
Flow Chart: LSU, Oxygen Sensor Heater Control Upstream Catalyst (SULEV calibration)



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Flow Chart: LSF1/LSF2, Oxygen Sensors downstream catalyst

SULEV applications



**.08.00.00 EGR Monitoring**

Not applicable

**.09.00.00PCV MONITORING**

The PCV system assures that no gas from the crankcase system escapes into the atmosphere.

All connectors which are not necessary to open during typical maintenance / repair actions are implemented as hard to open.

All easy to open connectors are monitored by the OBD system.

**.10.00.00ENGINE COOLANT SYSTEM MONITORING**

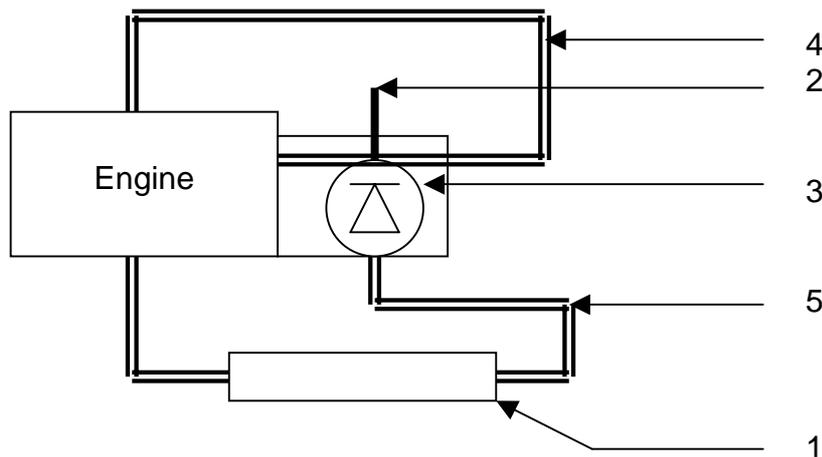
**.10.01.00 General description**

The engine cooling system consists of five main parts.

1. The Engine Cooler
2. The Engine Coolant Temperature Sensor
3. The Thermostat Valve
4. The small Cooling Circuit
5. The large Cooling Circuit

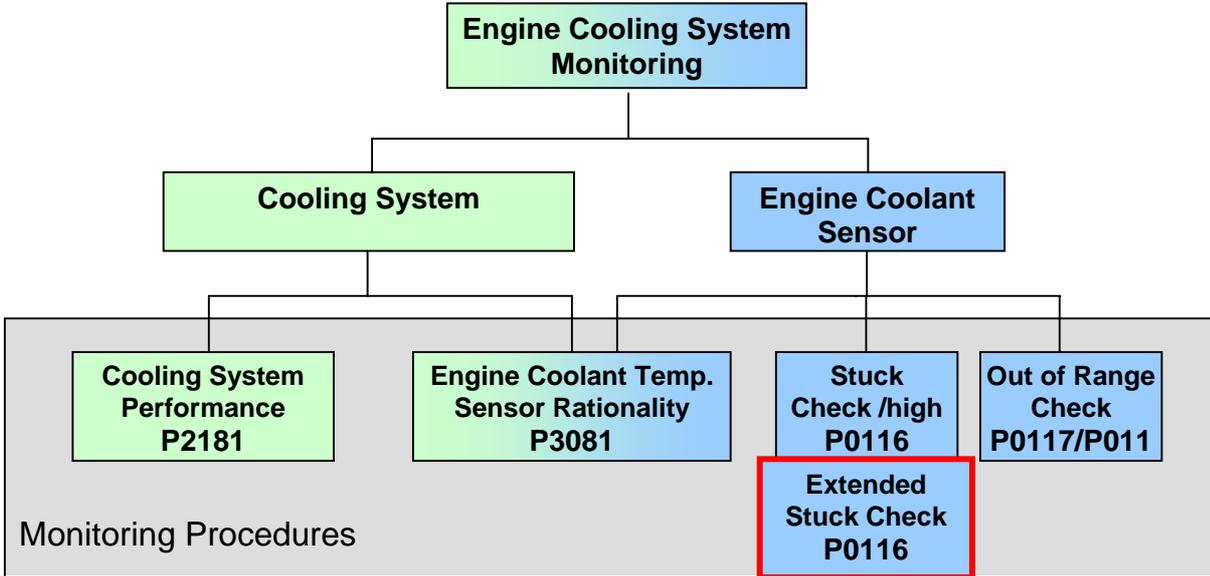
During heating up the Engine the coolant flows first inside the small cooling circuit. After the coolant reach a sufficient temperature the thermostat valve will open the large cooling circuit to integrate the engine cooler.

The engine coolant temperature sensor measures a mixed temperature between the coolant coming from the small and large cooling circuit.

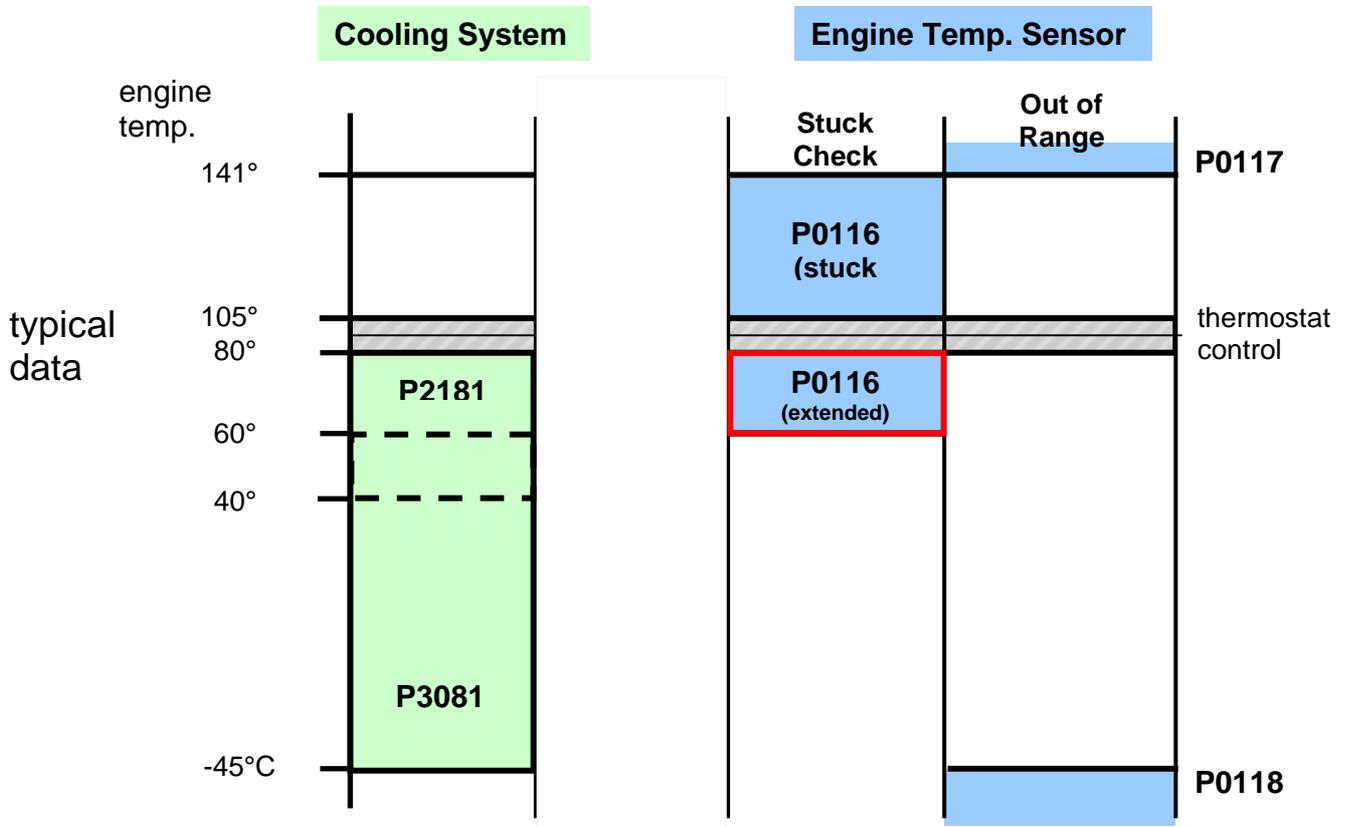


.10.01.02 Monitor Functional Description

The engine cooling system-monitoring strategy consists of two main diagnostic parts.



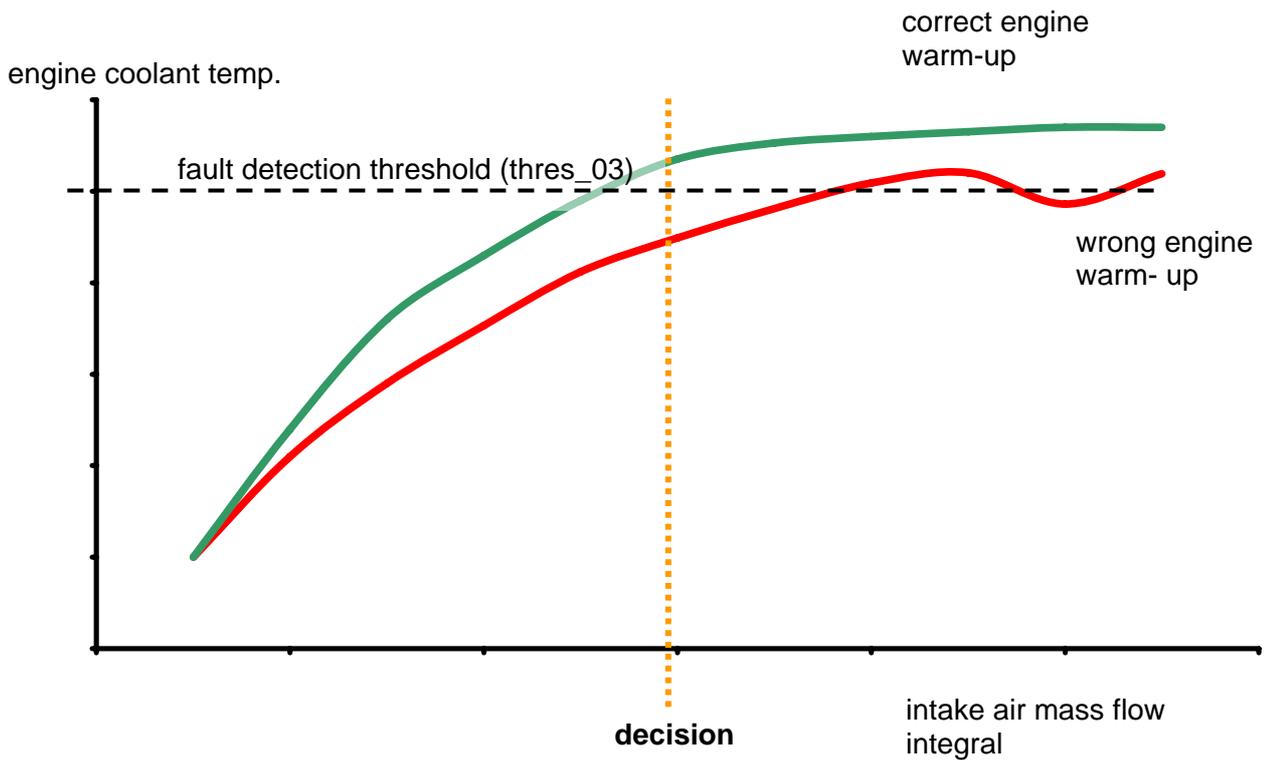
Each of the engines cooling monitoring function has its own special engine temperature range in which it will be enabled.



.10.03.00 Charts and Flow Charts

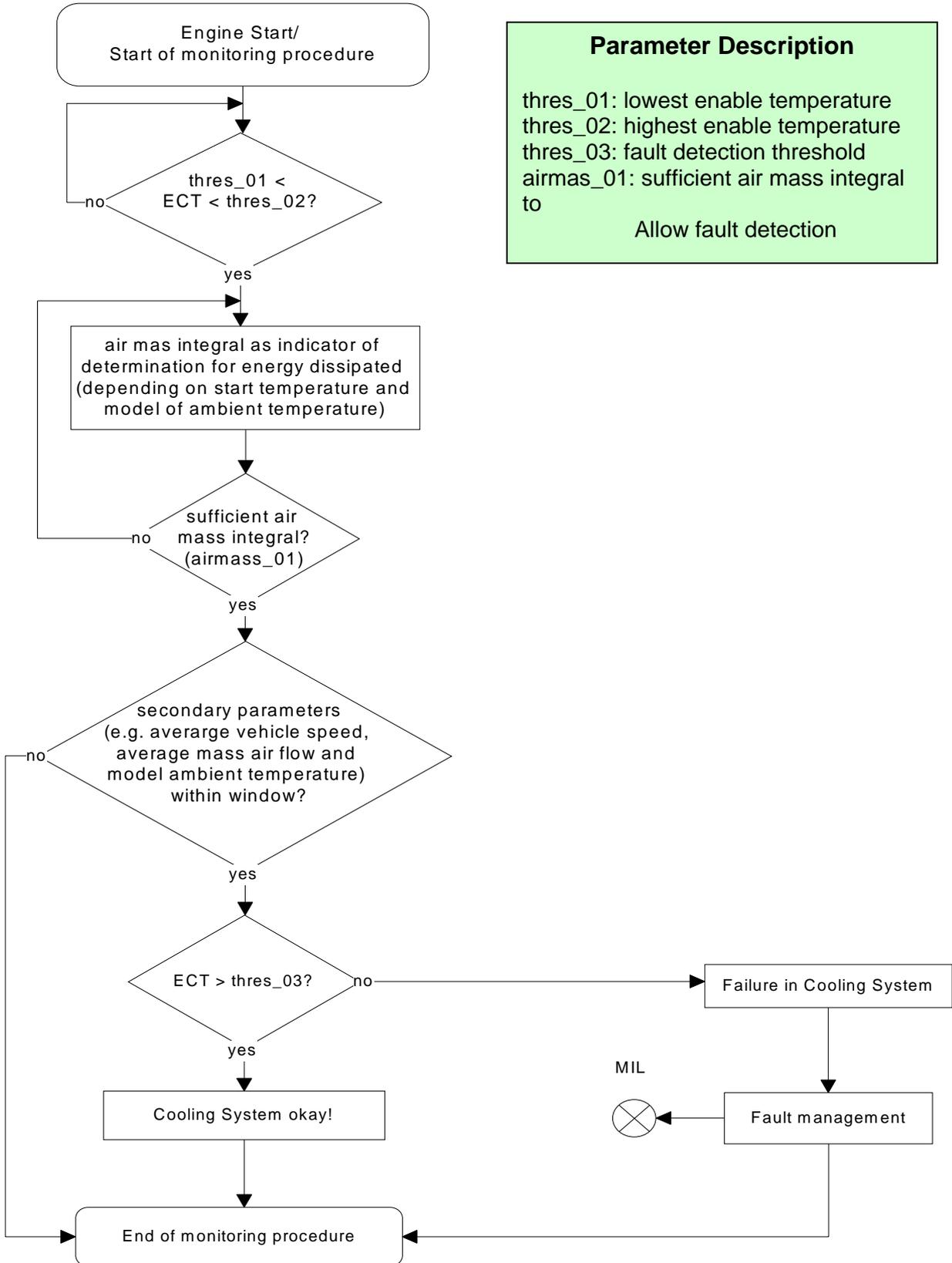
Cooling System Performance (P2081)

In case that the engine coolant temperature does not reach a certain value after a sufficient mass air flow under normal driving conditions, the cooling system performance is considered to be reduced.



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Flow Chart Cooling System Performance (P2081)



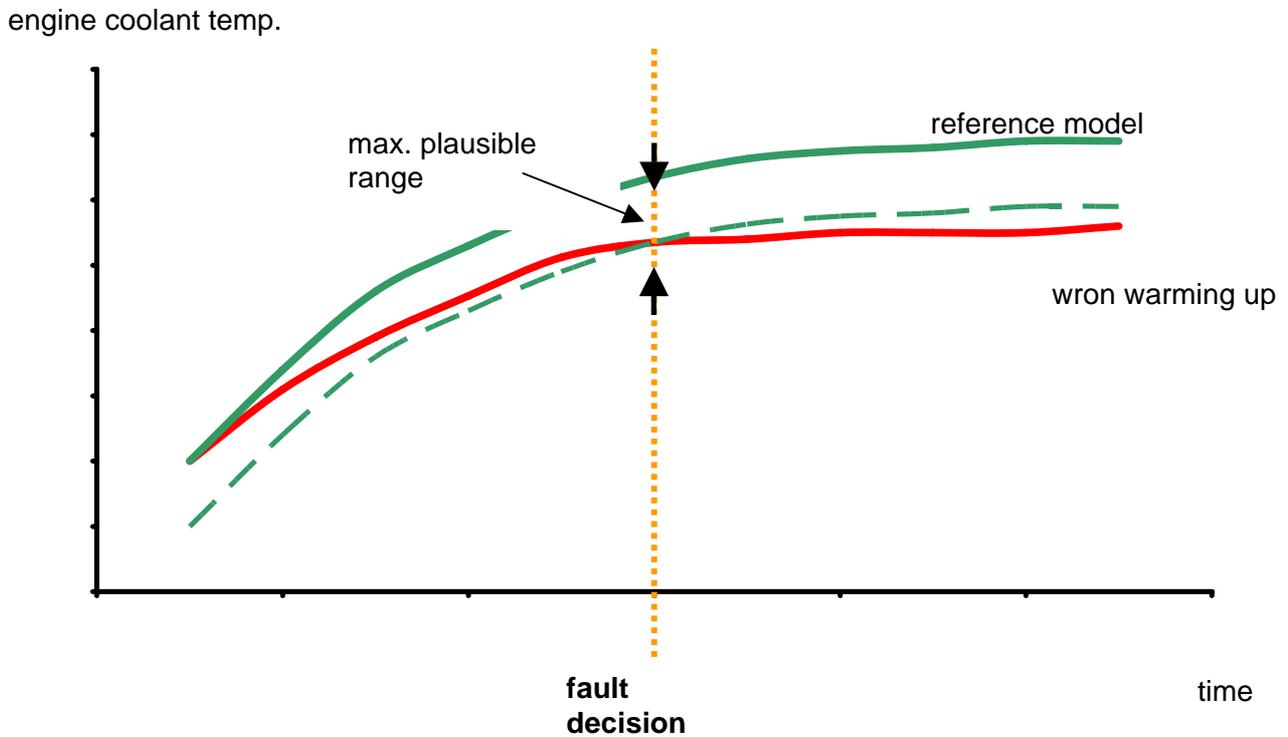
**Parameter Description**

thres\_01: lowest enable temperature  
 thres\_02: highest enable temperature  
 thres\_03: fault detection threshold  
 airmas\_01: sufficient air mass integral to  
 Allow fault detection

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

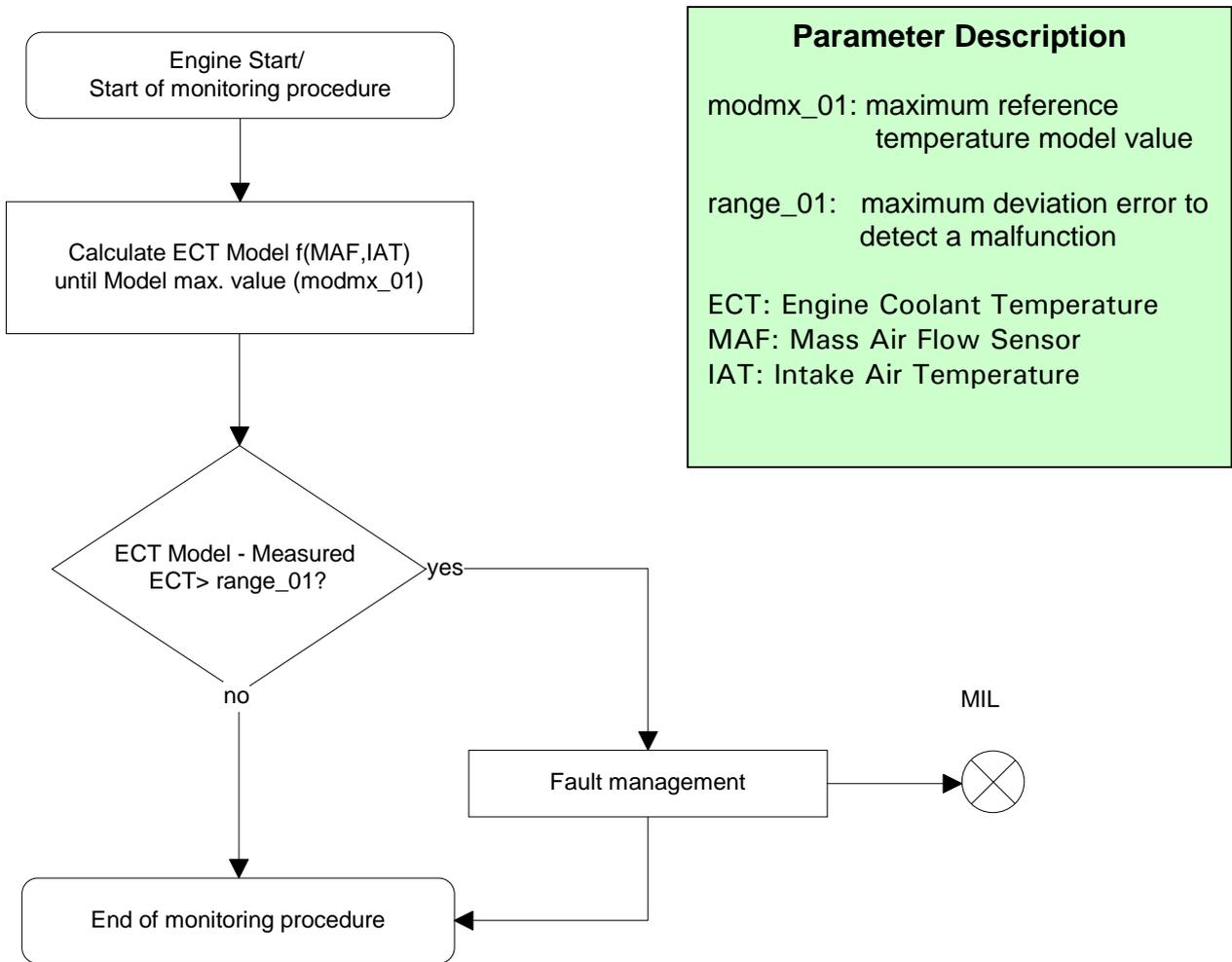
### Engine Coolant Temp. Sensor Rationality (P3081)

In case that the engine coolant temperature does not fit to a reference model temperature in a certain range, the cooling system is defective or the sensor is not in a plausible range.



## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

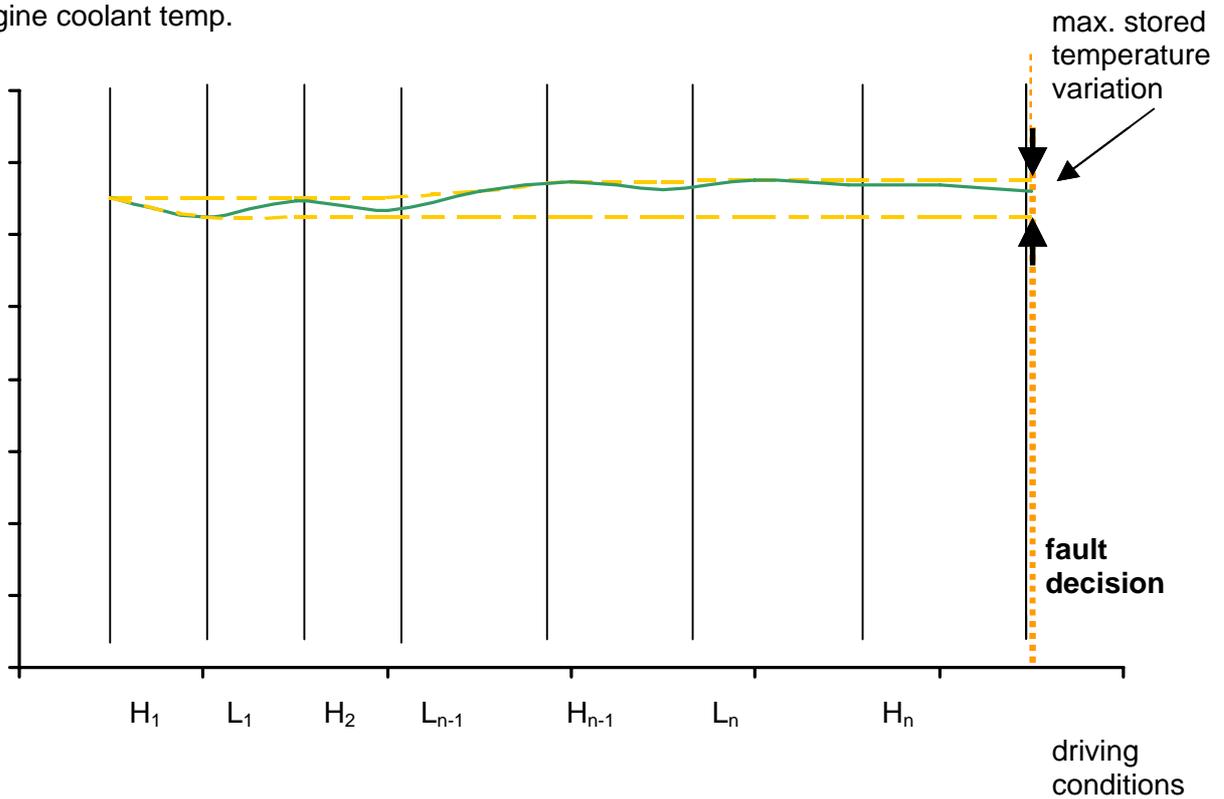
Flow Chart Coolant Temperature Sensor Rationality (P3081)



**Engine Coolant Temperature Sensor Stuck High (P0116)**

After engine start the system stores continuously the lowest and highest ECT above the thermostat control temperature for a driving cycle. In case that after several driving conditions the difference between ECT max and ECT min is lower than the threshold the sensor stuck at high values.

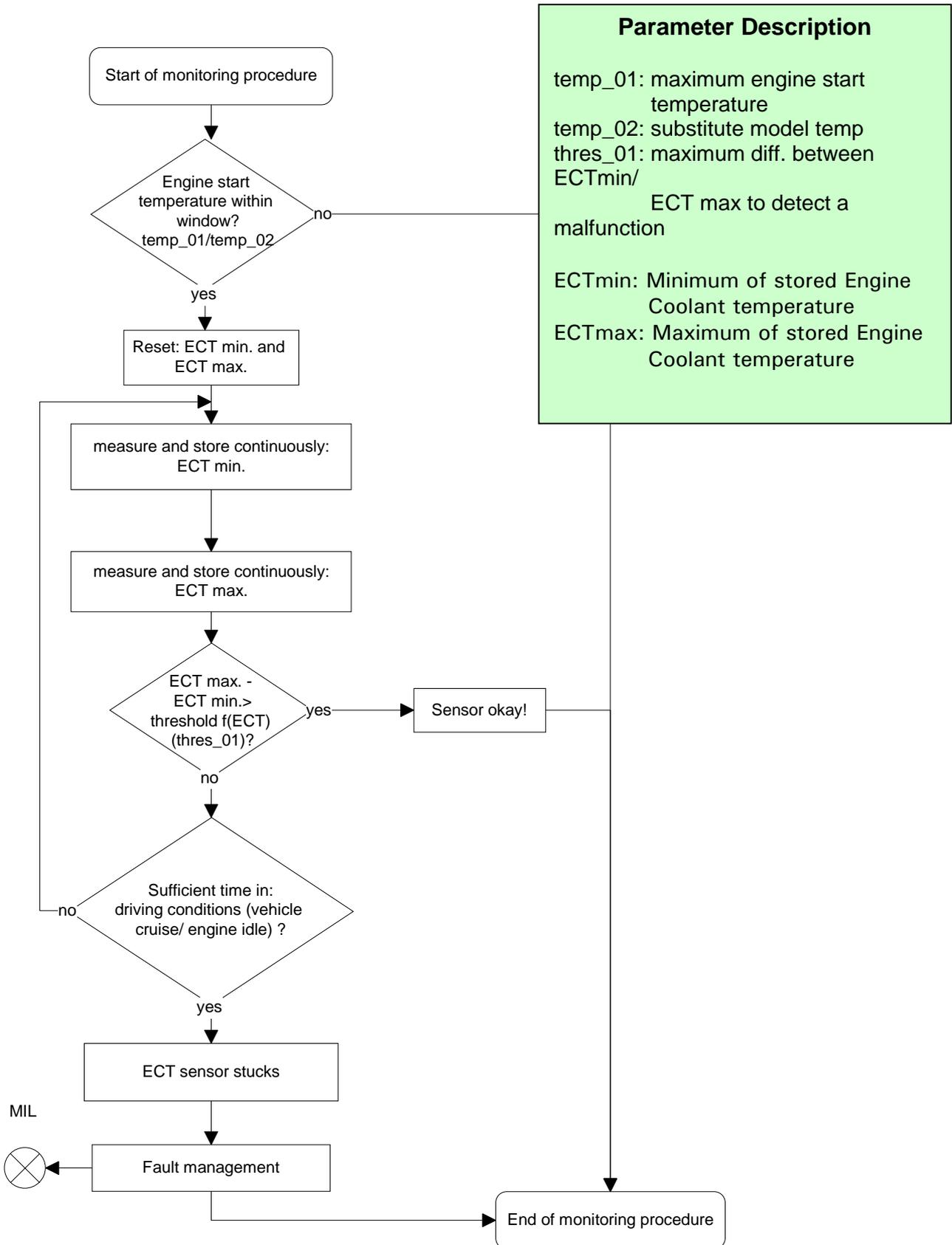
engine coolant temp.



H: driving condition with high cooling performance (vehicle cruise)

L: driving conditions with low cooling performance (idle)

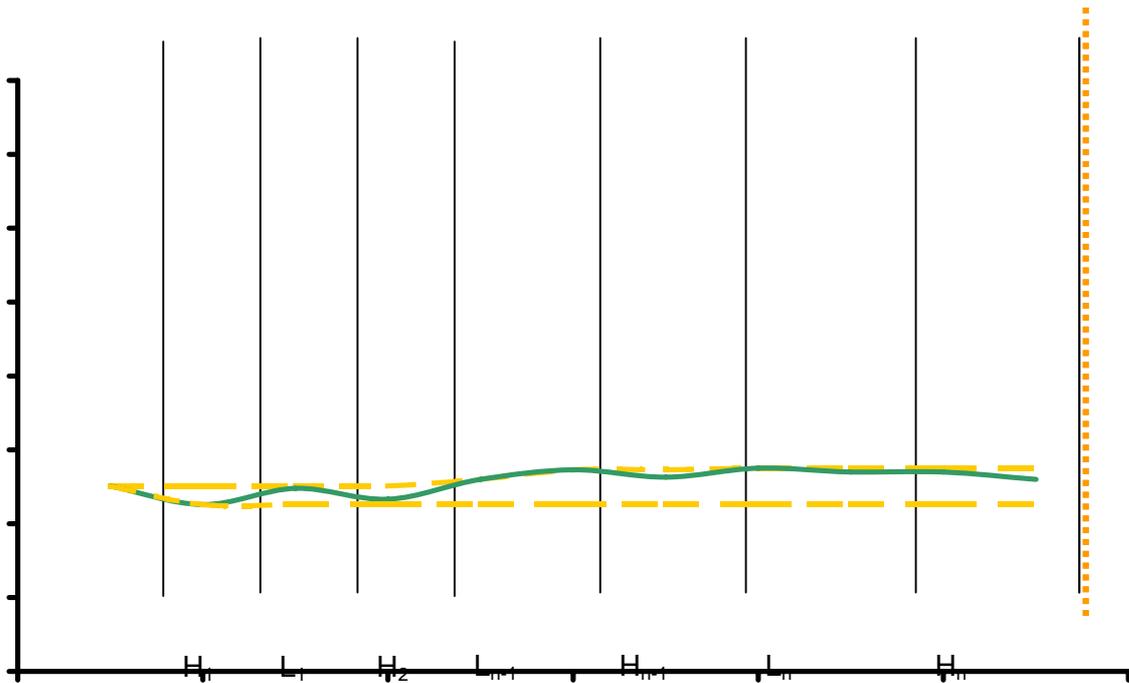
Flow Chart Engine Coolant Temperature Sensor Stuck High (P0116)



**Engine Coolant Temperature Sensor Stuck Low (P0116)**

After engine start the system stores continuously the lowest and highest ECT below the thermostat control temperature for a driving cycle. In case that after several driving conditions the difference between ECT max and ECT min is lower than the threshold the sensor stuck at low values.

engine coolant temp.

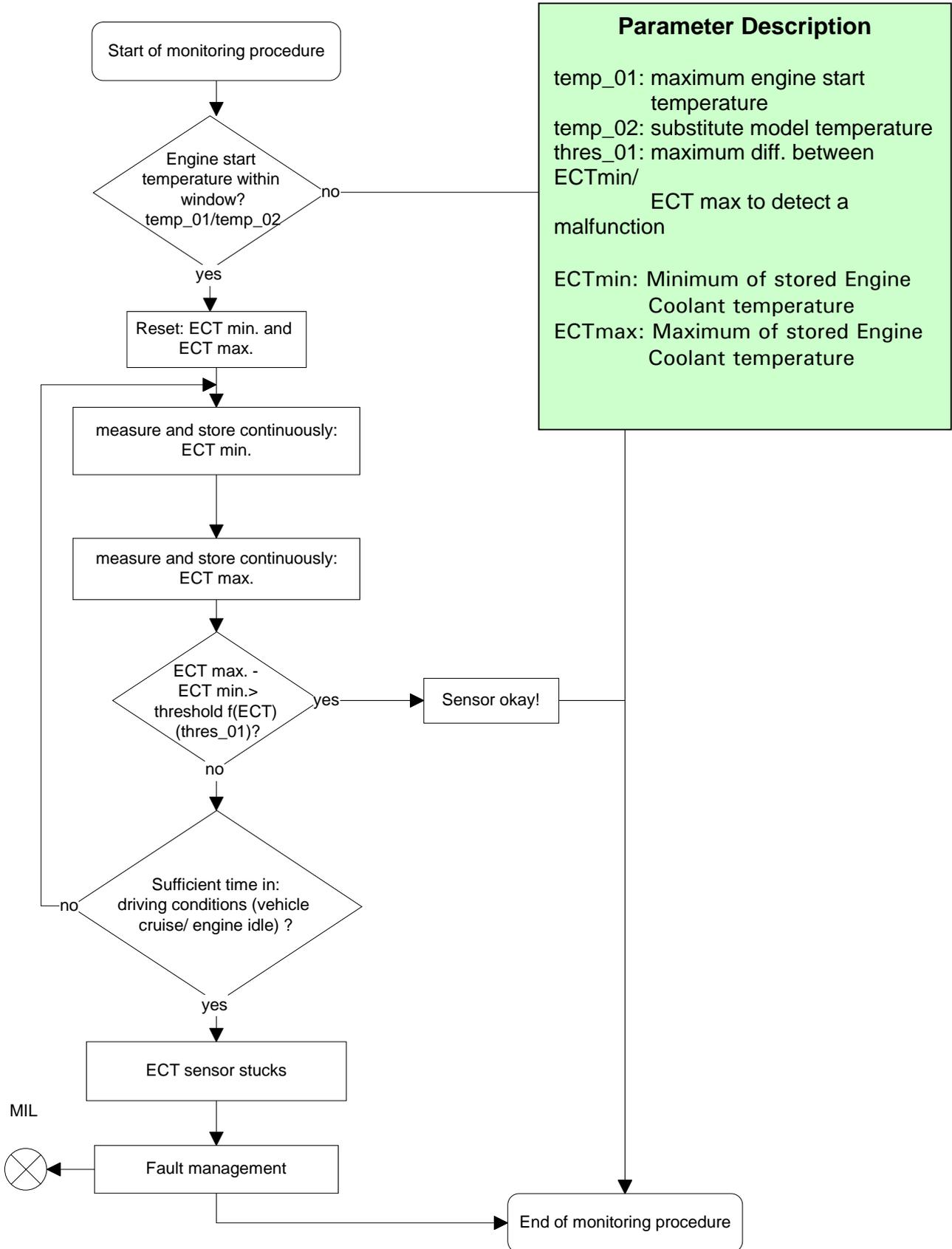


H: driving condition with high cooling performance (vehicle cruise)

L: driving conditions with low cooling performance (idle)

# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

## Flow Chart Engine Coolant Temperature Sensor Stuck Low (P0116)

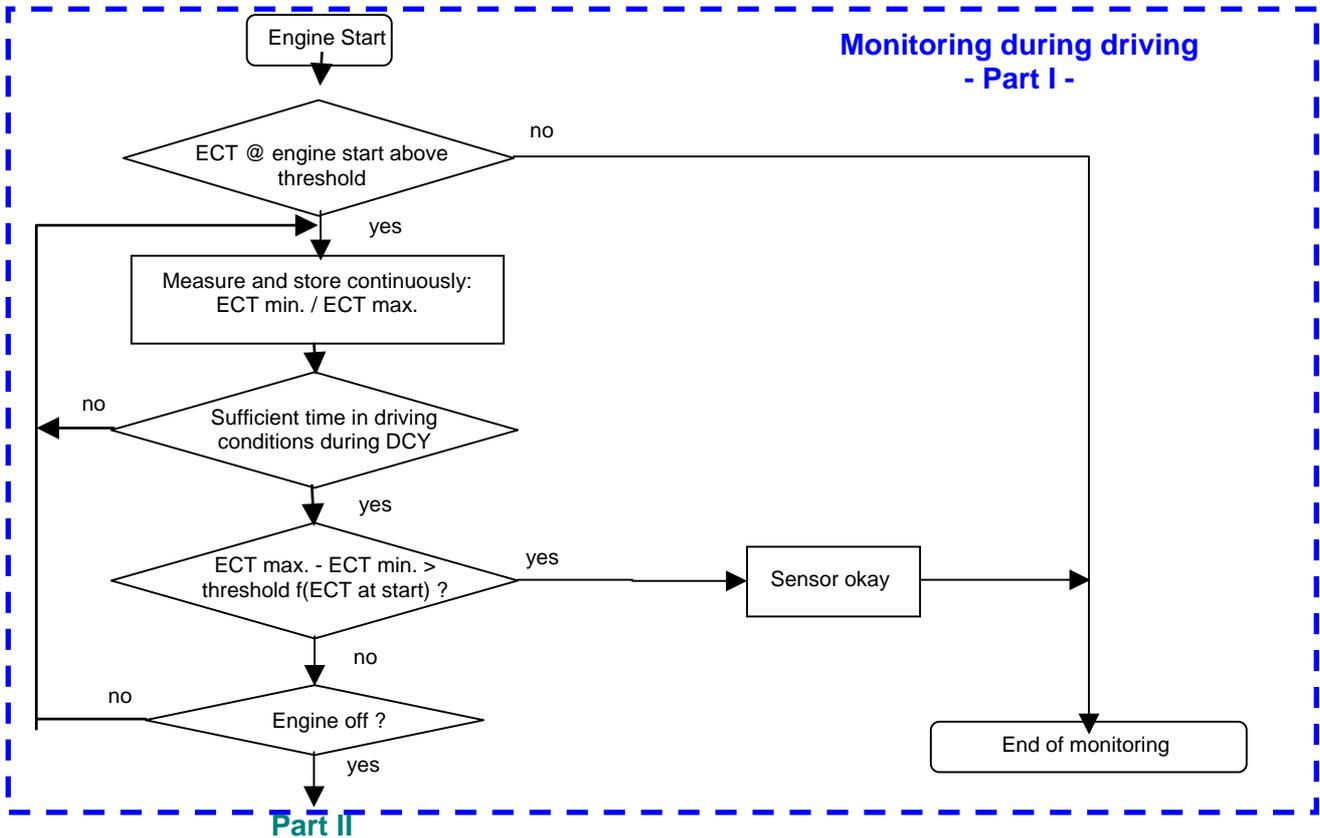


## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Flow Chart Engine Coolant Temperature Sensor Stuck Test (all temperatures above threshold) (P0116)

Monitoring of engine temperature during normal DCY and during engine shut off time

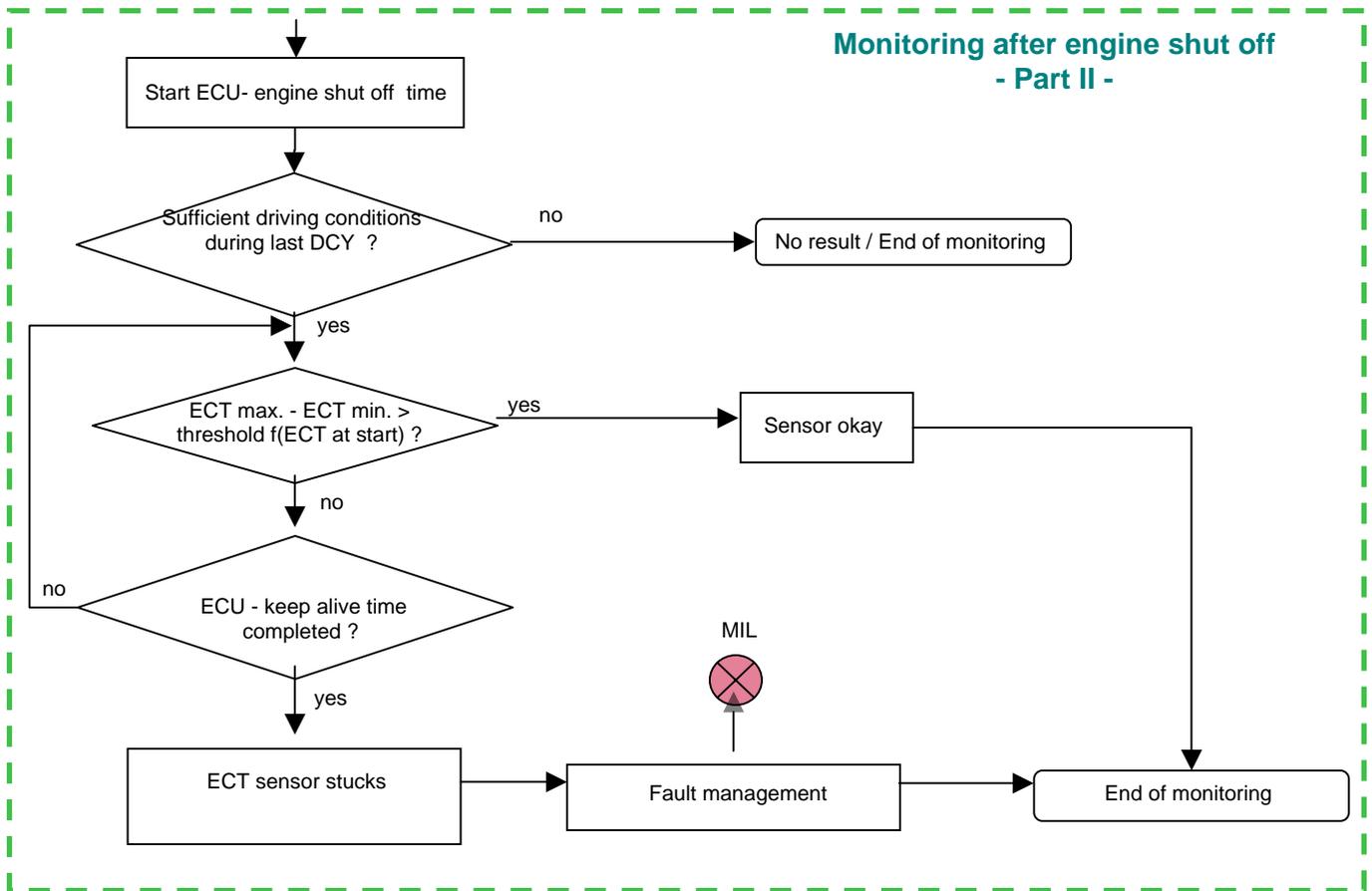
Part I:



# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Monitoring of engine temperature during normal DCY and during engine shut off time

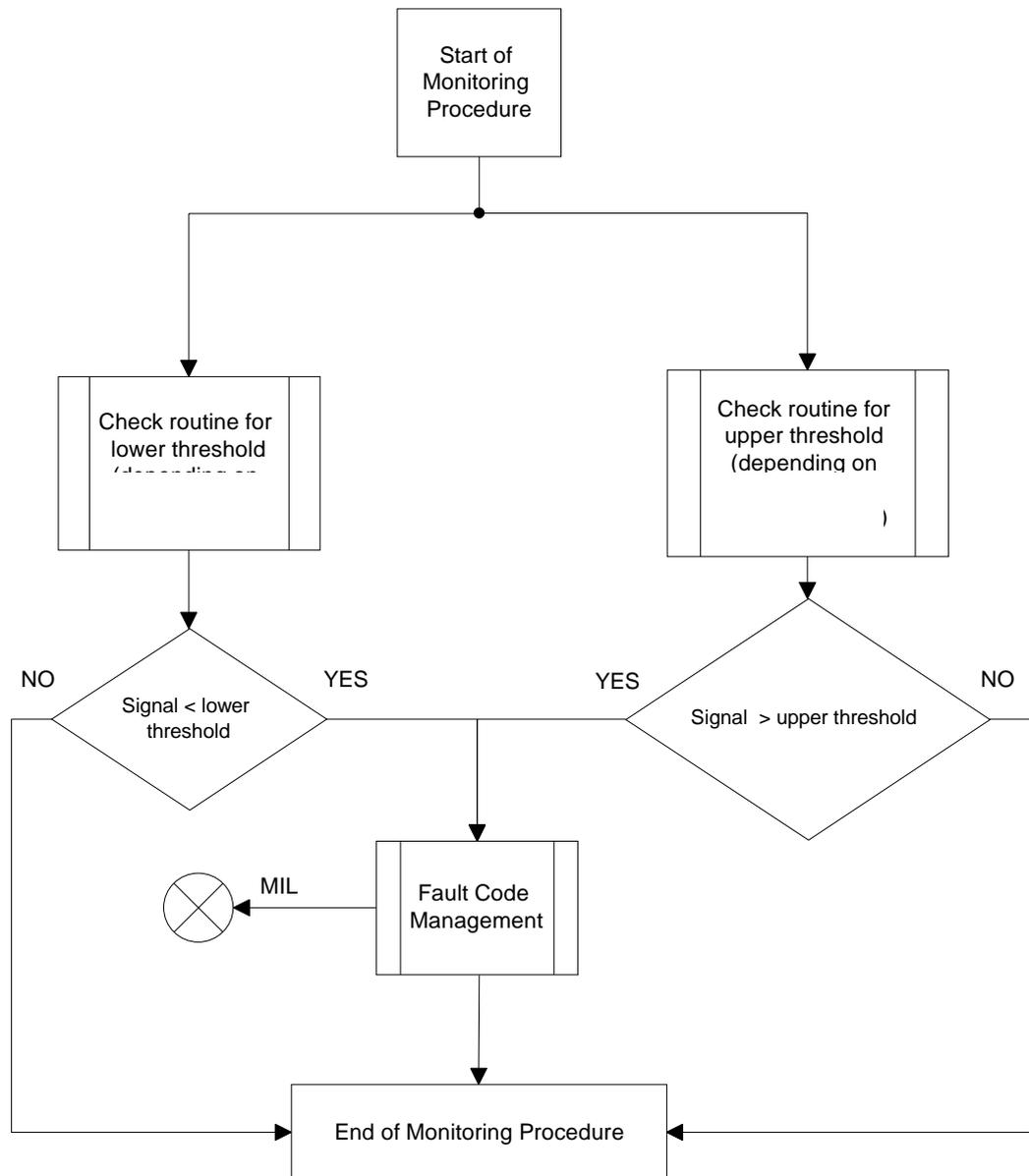
Part II:



**Engine Coolant Temperature Sensor Out of Range Check (P0118 / P0117)**

### Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

The signal of Engine Coolant Temperature Sensor is evaluated and considered to be electrically out of range if either the upper or the lower thresholds is exceeded.



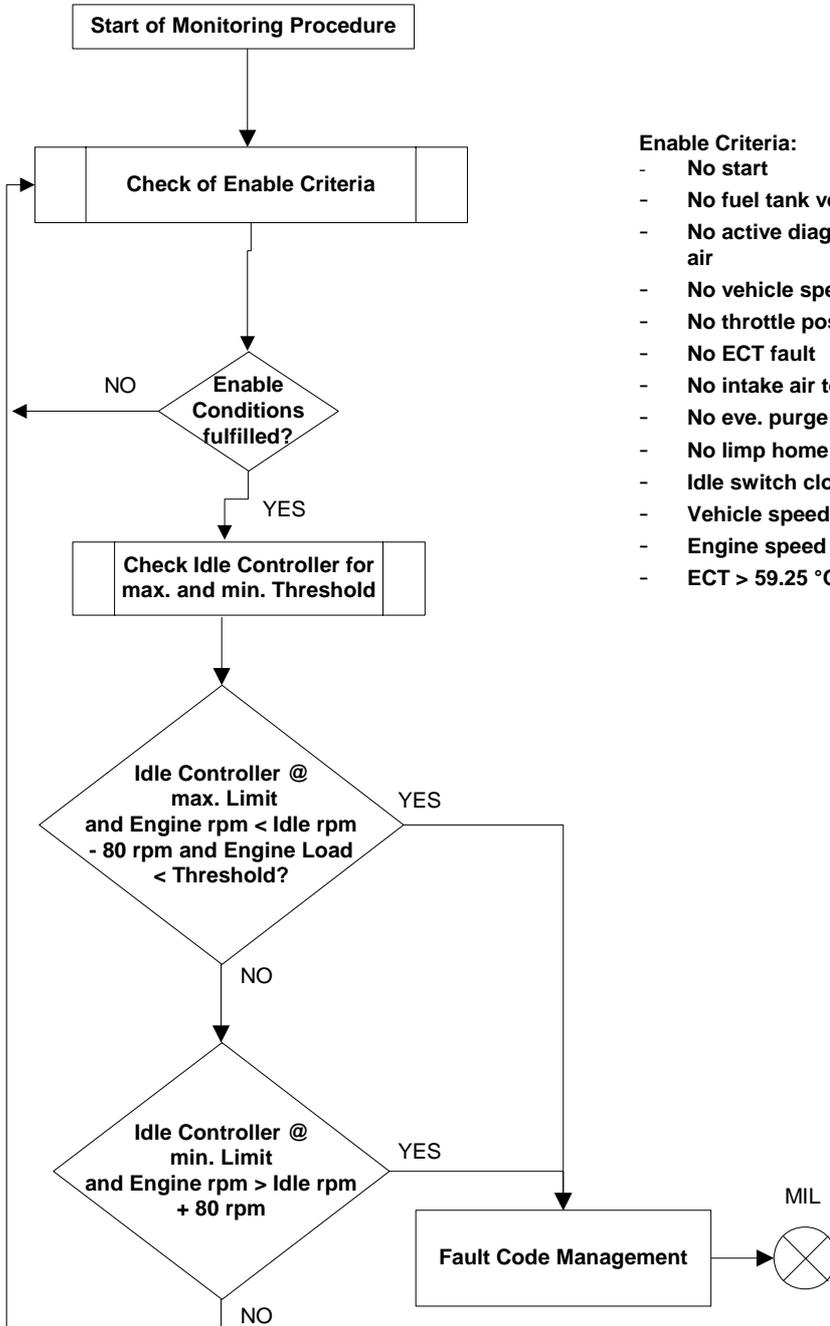
**Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

- .11.00.00**      **COLD START EMISSION REDUCTION STRATEGY MONITORING**  
Not applicable
- .12.00.00**      **AIR CONDITIONING (A/C) SYSTEM COMPONENT MONITORING**  
Not applicable
- .13.00.00**      **VARIABLE VALVE TIMING AND/OR CONTROL (VVT) SYSTEM MONITORING**  
Not applicable
- .14.00.00**      **DIRECT OZON REDUCTION (DOR) SYSTEM MONITORING**  
Not applicable
- .15.00.00**      **PARTICULATE MATER (PM) TRAP MONITORING**  
Not applicable
- .16.00.00**      **COMPREHENSIVE COMPONENTS MONITORING**  
Flow Charts in addition to the summary table explanations:
- .16.01.00**      **Injection Valve**  
Check is performed while using Output Stage Check 16.09.12:
- .16.02.00**      **Fuel Pump Relay**  
Check is performed while using Output Stage Check 16.09.12:

# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

## .16.03.00 Idle Controller

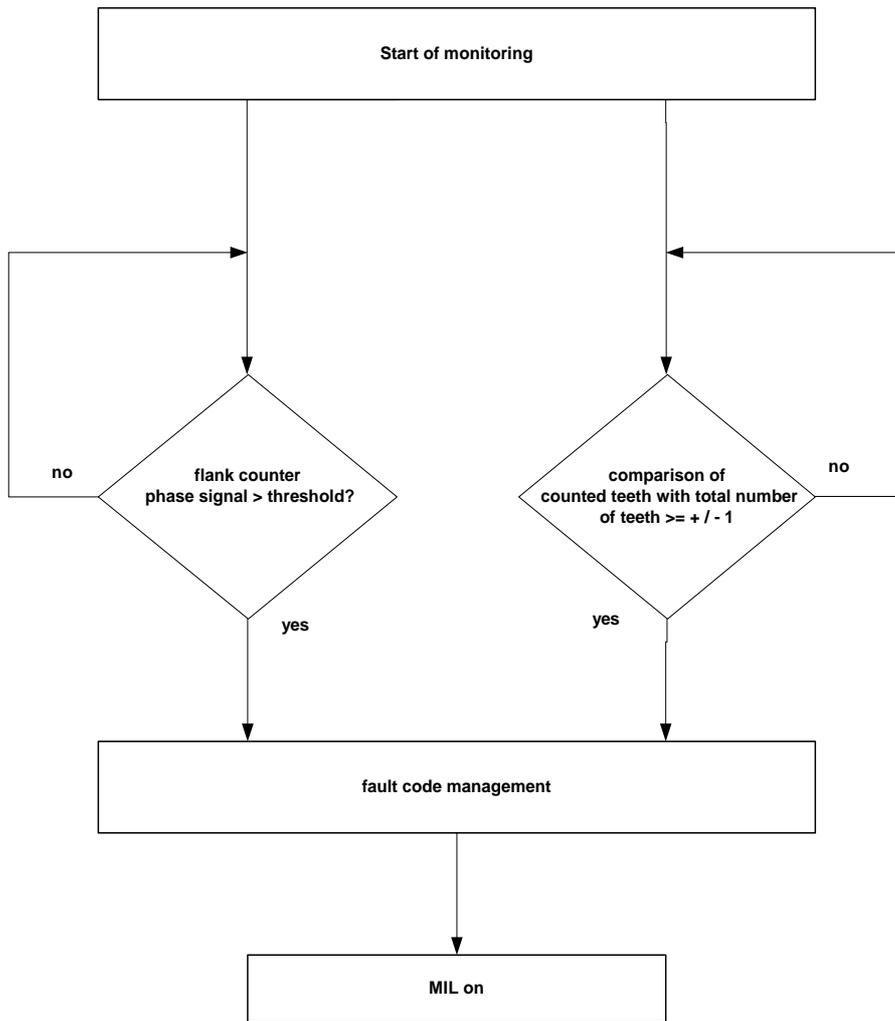
(Idle Control Check)



### Enable Criteria:

- No start
- No fuel tank ventilation with high degree of saturation
- No active diagnosis of EVAP system and secondary air
- No vehicle speed fault
- No throttle position fault
- No ECT fault
- No intake air temperature fault
- No eve. purge valve fault
- No limp home of engine speed sensor
- Idle switch closed
- Vehicle speed = 0 mph
- Engine speed @ idle
- ECT > 59.25 °C

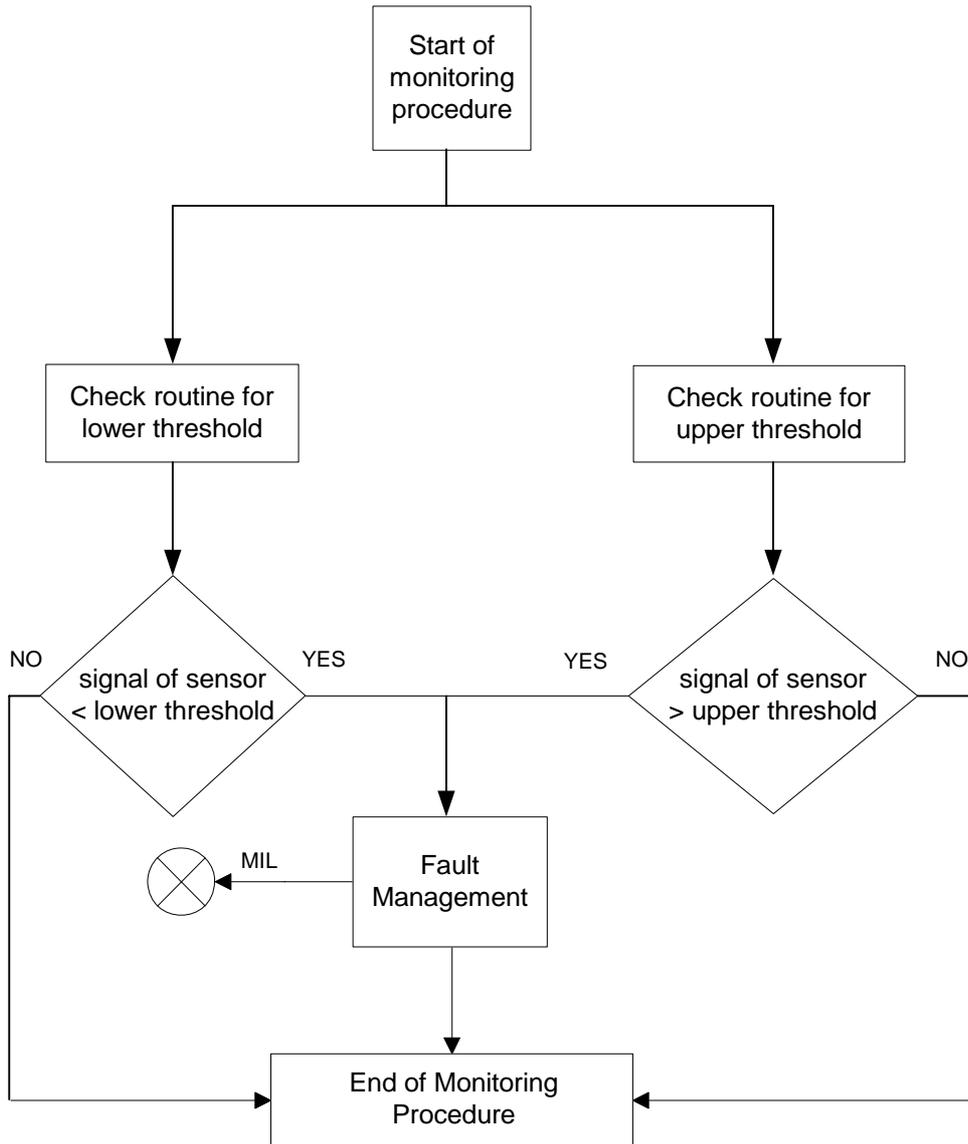
.16.04.00 ..... **Engine Speed Sensor:**



.16.05.00 ..... **Warm-up Bypass valve:**  
(Not applicable)

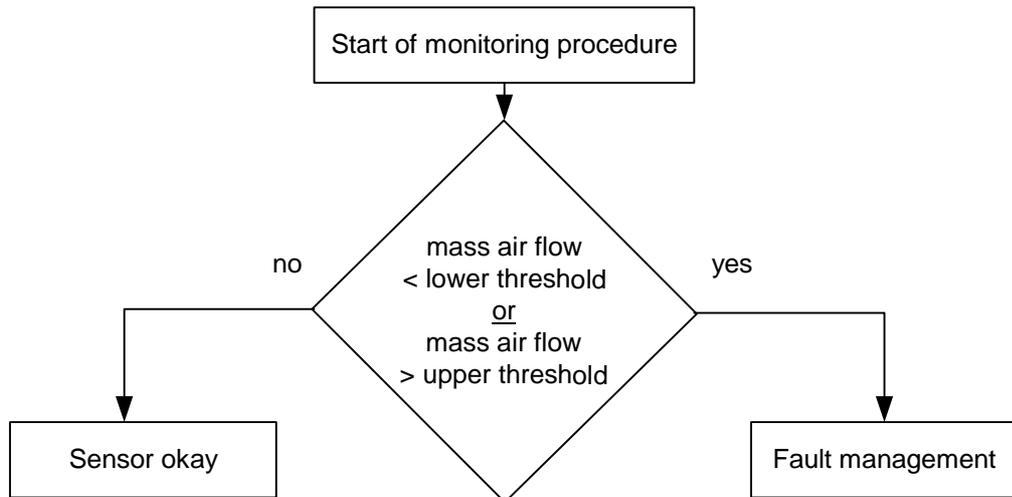
.16.06.00      Signal Range Check for different sensor

IAT  
MAF  
ECT  
Camshaft position sensor  
Charge pressure control valve

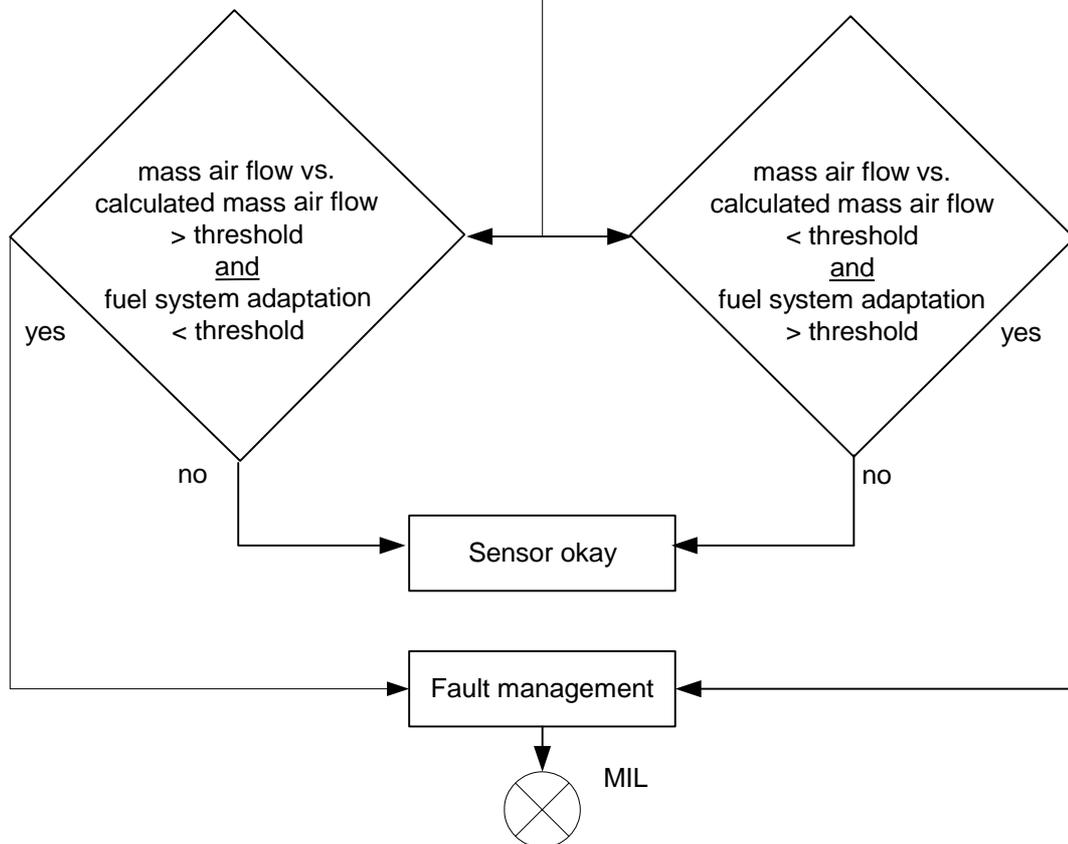


.16.07.00 ..... Rationality Mass Air Flow Sensor (MAF)

One MAF Sensor System:

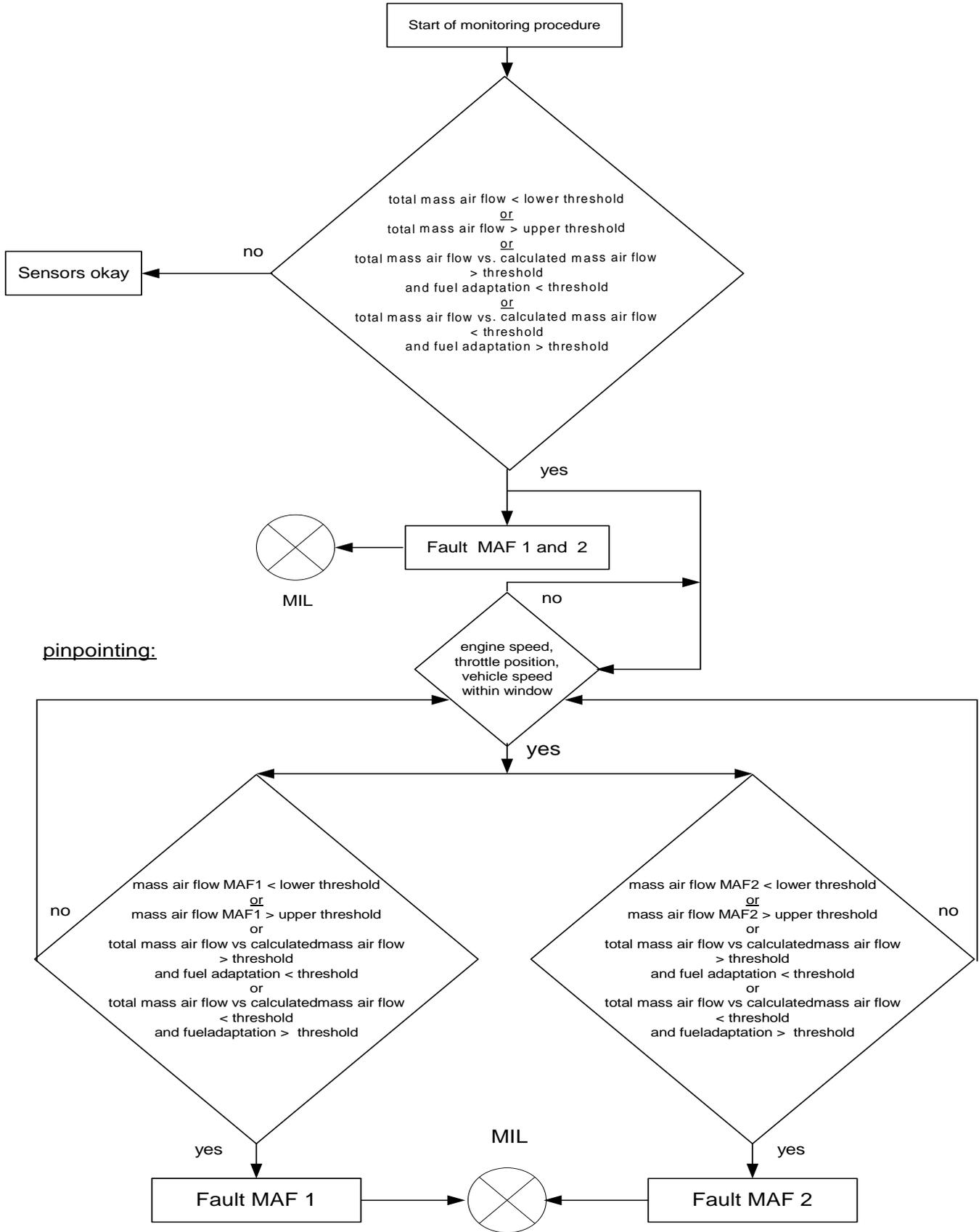


additional options for some calibrations:

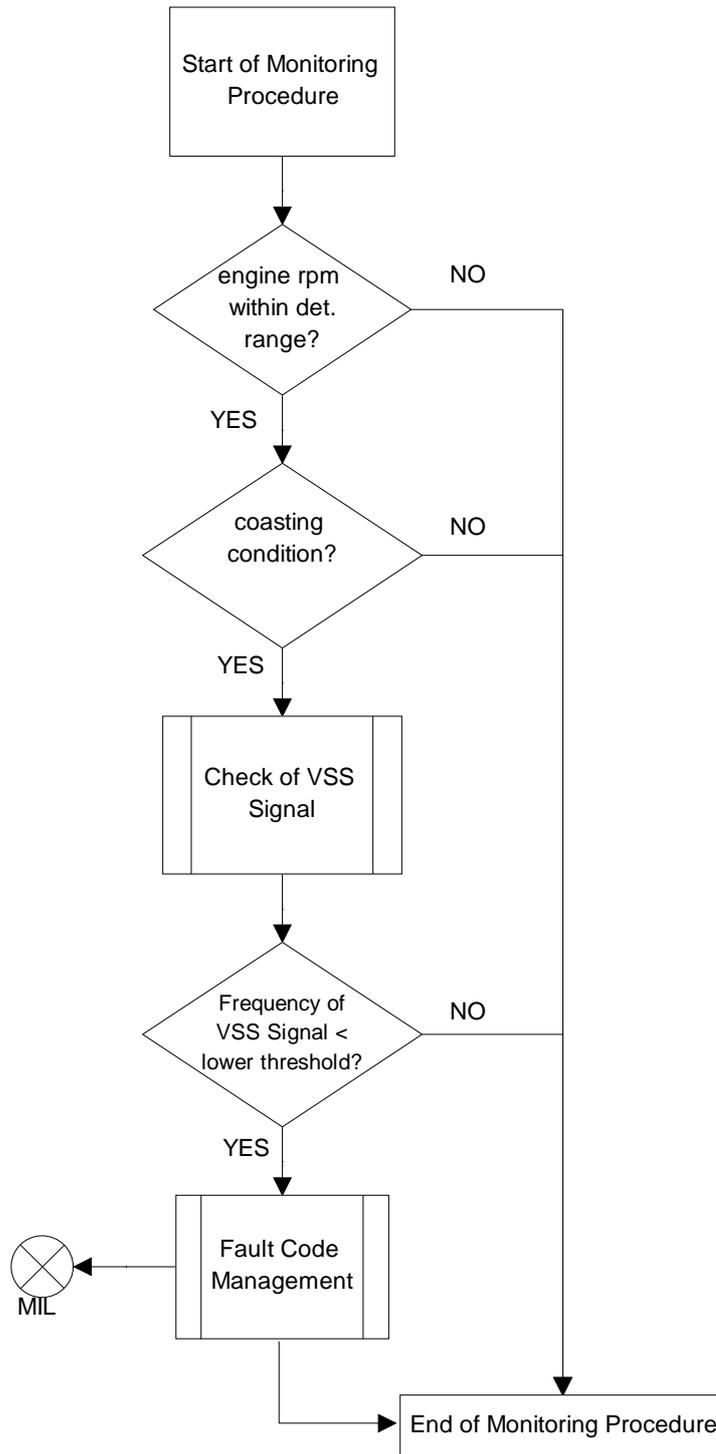


# Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

Two MAF Sensors System:

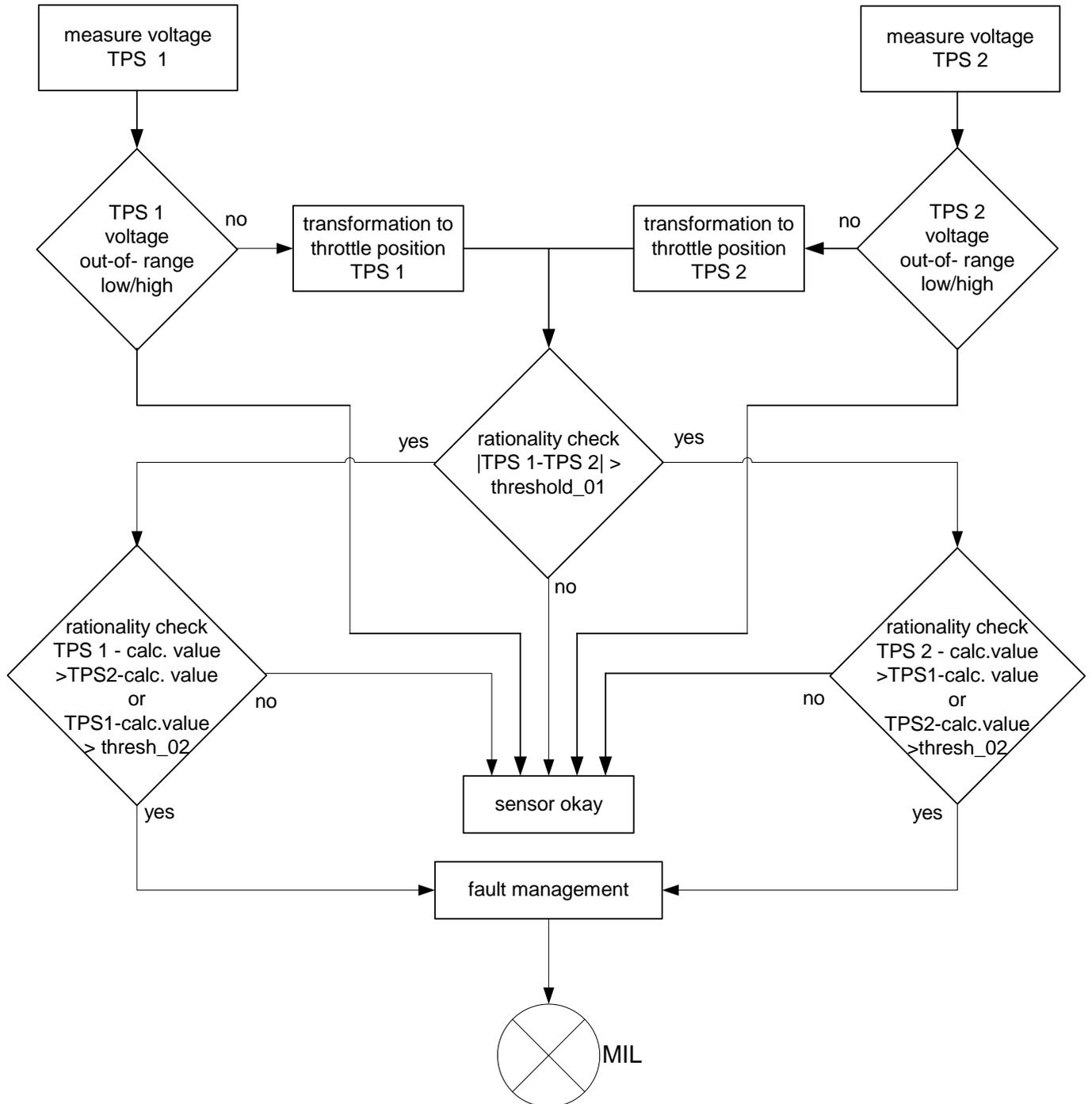


.16.08.00 Vehicle Speed Sensor (VSS)

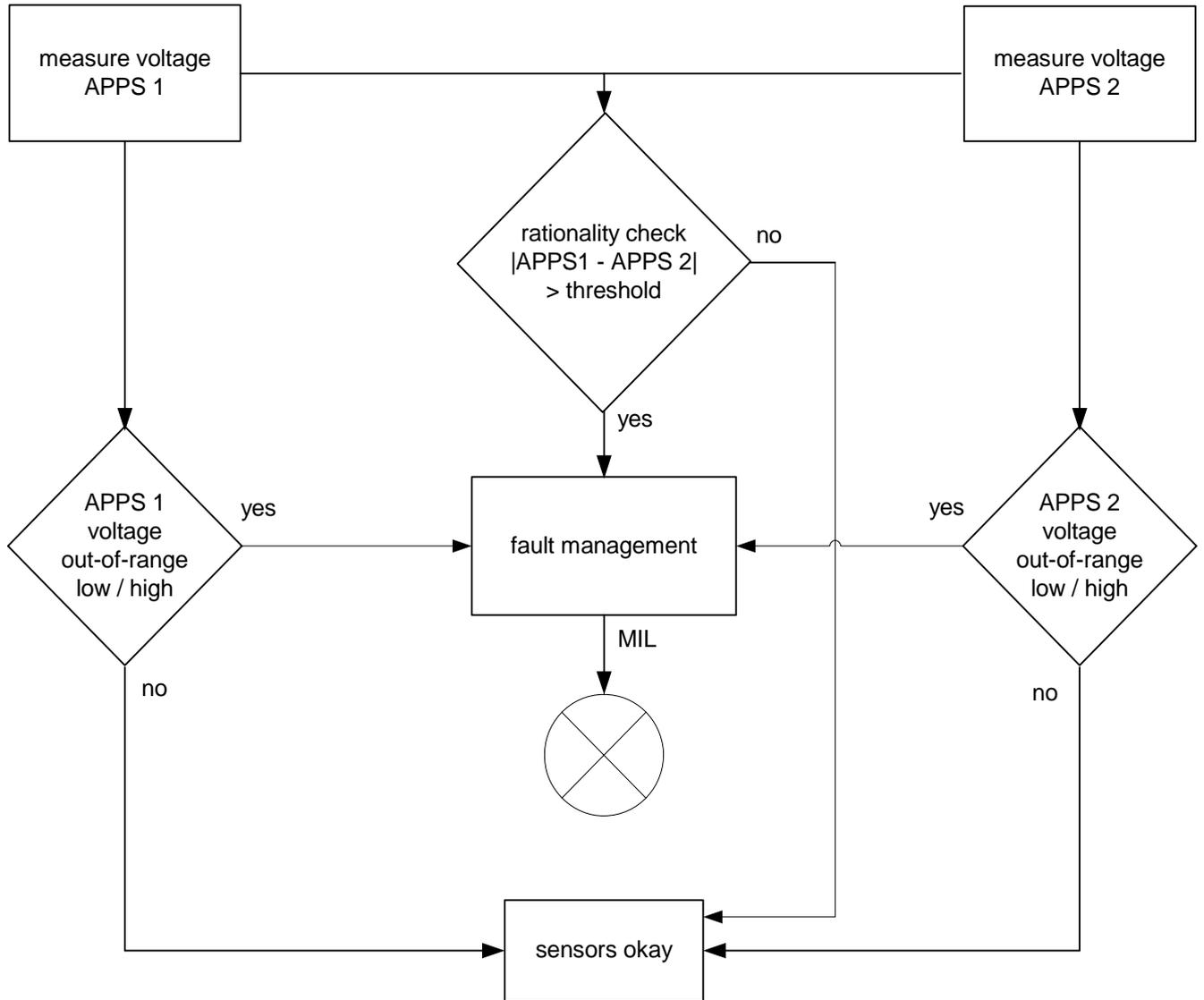


.16.09.00 Throttle Position Sensor (throttle unit with E-gas actuator)

The throttle body consists of two potentiometers (reversed voltage logic). During the first start, the potentiometer characteristics are adapted and stored. The diagnostic monitors the corrected values of potentiometer 1 and 2. In the case of a higher difference than a threshold value both signals are compared to the engine load to determine and disable the faulty one. A fault code will be stored and the MIL will be illuminated.

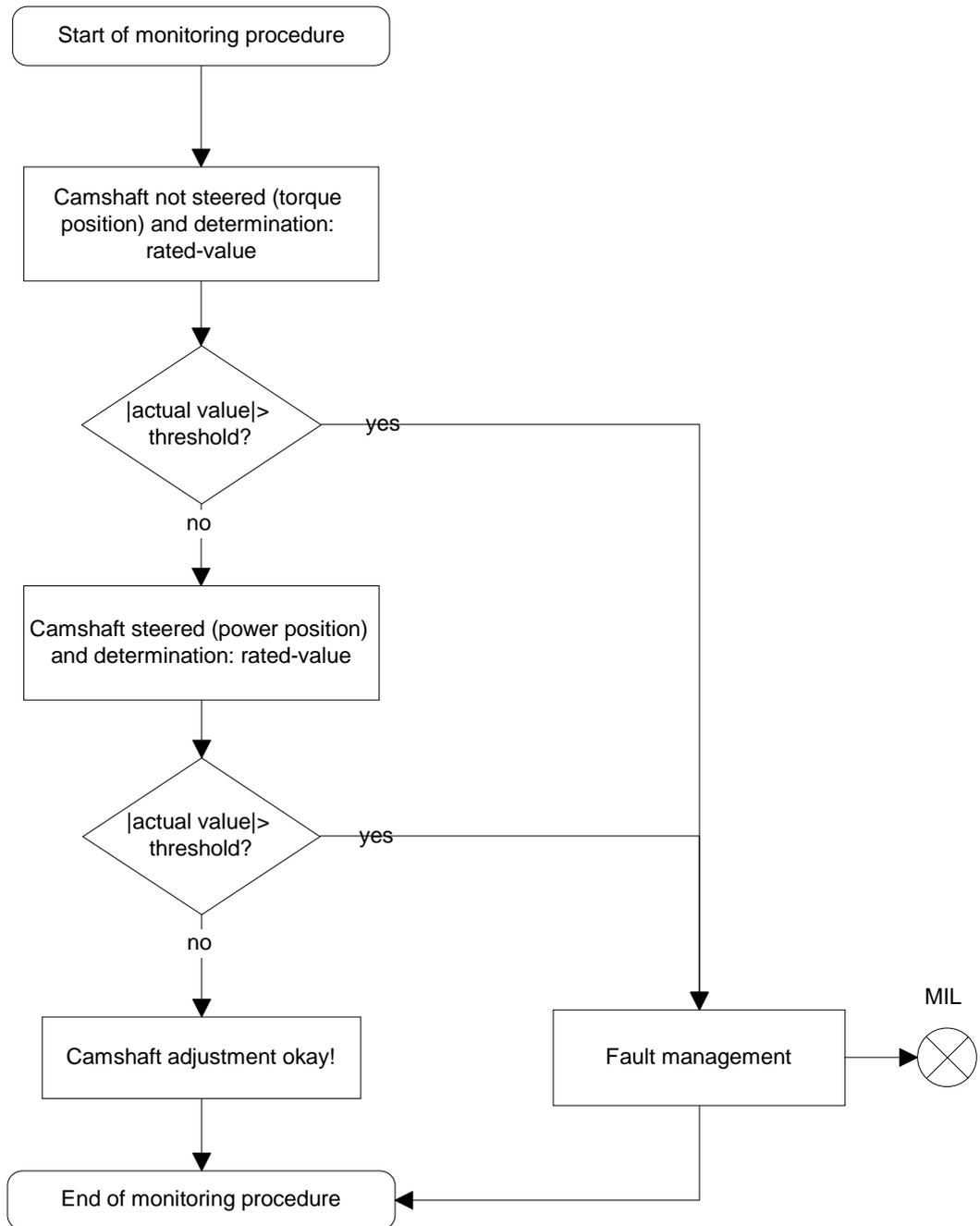


.16.10.00 Accelerator pedal position sensor (APPS)

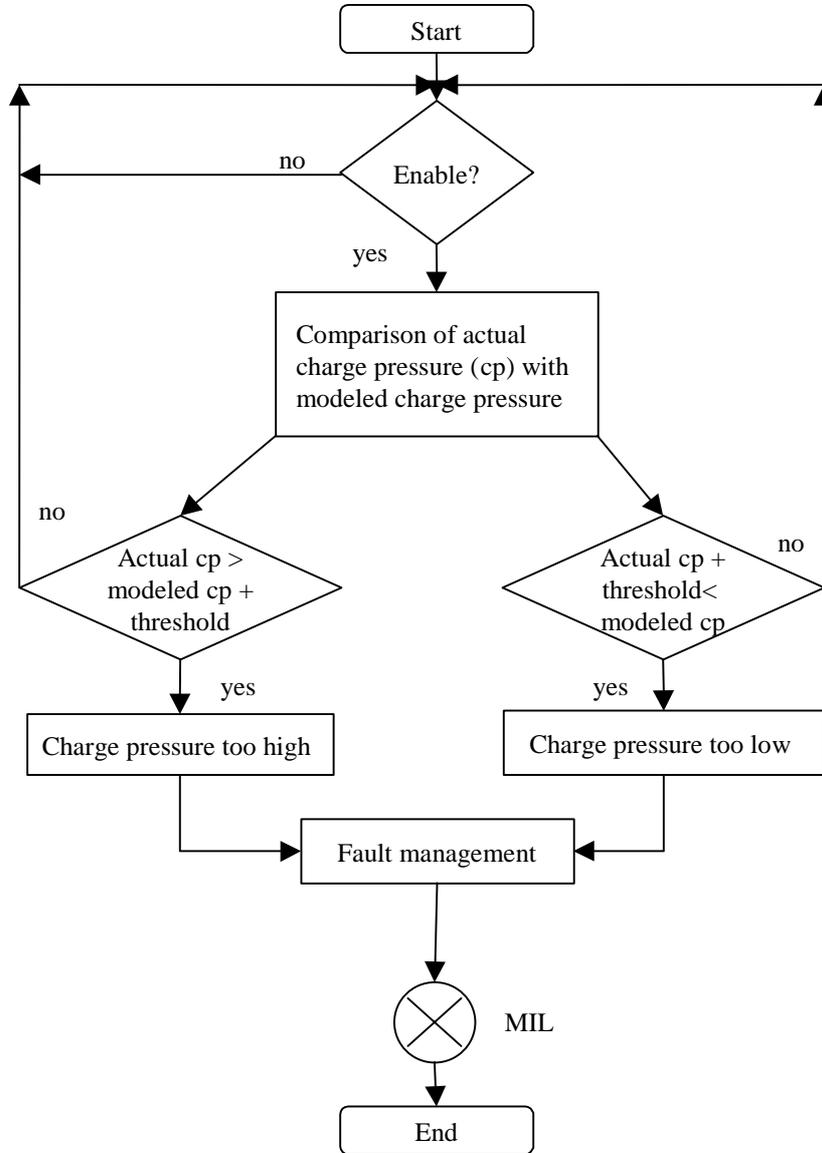


.16.11.00 ..... Camshaft Position Sensor

Camshaft Position Monitor

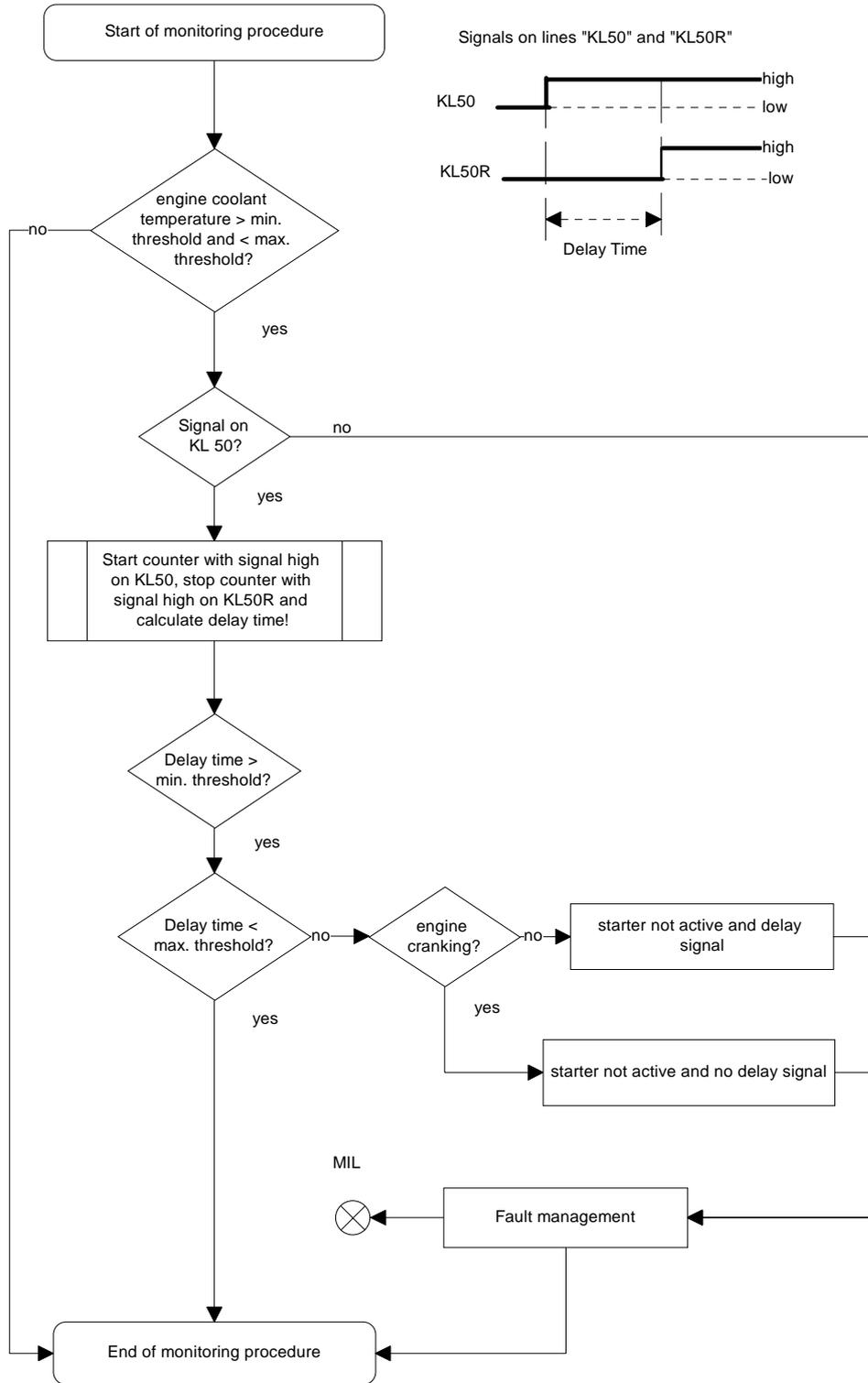


.16.12.00 Boost Pressure Control Valve



.16.13.00 Engine Start Delay Relay (SULEV)

Engine Start Delay Relay



**.16.14.00 Exhaust Temperature Sensor (SULEV)**

**.16.14.01 General Monitoring Description**

The exhaust temperature sensor (ETS) is monitored for rationality during engine cold start, where engine coolant temperature, intake air temperature and exhaust temperature are expected within the same temperature range ("stuck high" check).

**.16.14.02 Monitor function description**

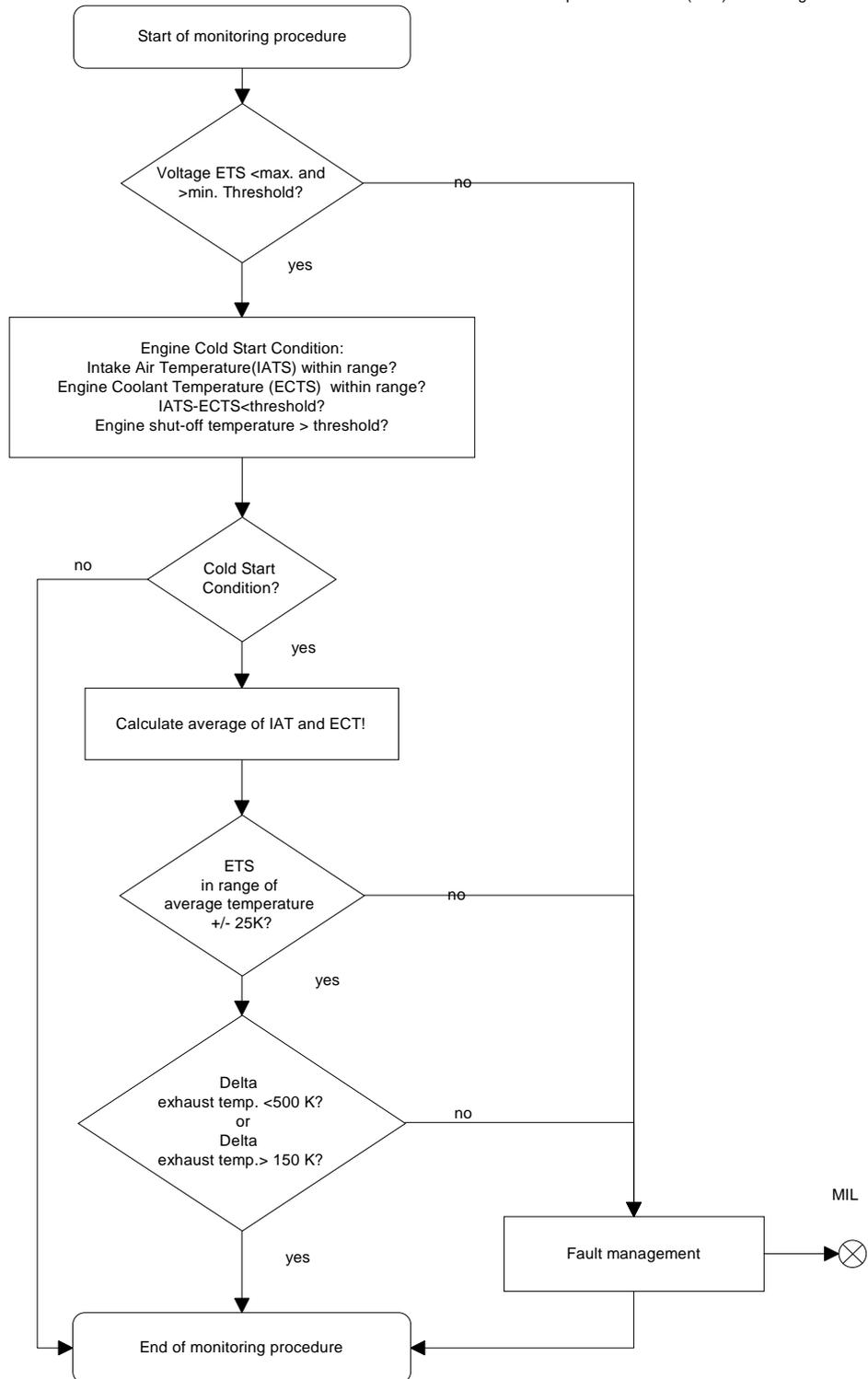
After engine has been cold started the slope of ETS is monitored and should not be higher than a max. Threshold and not lower than a min. threshold.

Both plausibility checks are completed before the ETS information is used in other monitors (e.g. secondary air).

Additionally the final stage check monitors for shorts to ground or to battery.

.16.14.03 Chart(s) and Flow Chart (s)

Exhaust Temperature Sensor (ETS) Monitoring



## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

.16.15.00 ..... reserved

.16.16.00 ..... reserved

.16.17.00 ..... reserved

.16.18.00 ..... reserved

.16.19.00 ..... reserved

**.16.20.00 Automatic Transmission Monitor**

VW/Audi has different basic Automatic transmission systems. For each of these systems we are providing an OBD II summary table. Common OBD description from VW/Audi table TCM Groups show the references between transmission type and test groups.

**.16.21.00 Output Stage Check**

The output stages are integrated in manufacturer specific IC's:

The IC has a binary diagnostic line (e.g. SJ401).

If the control line of one stage has a different signal than the output line, the logic circuit inside the IC detects a malfunction. The logic circuit within the IC can separate the type of fault to a short circuit to minus, an open line, or a short circuit to plus. The check result will be sent to the ECM via diagnosis line.

**Signal tables of output stage check**

$U_{batt}=16V$	Normal working situations	Short circuit to ground	Short circuit to battery	Wiring Defective
$U_{in}$	Low high	High	Low	High
$U_{out} / I_{out}$	Low high	$<0.25-0.37 U_{Batt}$	$>2.2-3.0A$	$<0.65-0.84 U_{Batt}$
Fault detection	No fault	Fault	faut	faut

$U_{batt}=8V$	Normal working situations	Short circuit to ground	Short circuit to battery	Wiring Defective
$U_{in}$	Low high	High	Low	High
$U_{out} / I_{out}$	Low high	$<0.22-0.4 U_{Batt}$	$>2.2-3.0A$	$<0.54-0.78 U_{Batt}$
Fault detection	No fault	Fault	fault	fault

$U_{in}$  input voltage  
 $U_{out}$  output voltage  
 $I_{out}$  output current

**Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy**

**.17.00.00      OTHER EMISSION CONTROL OR SOURCE SYSTEM MONITORING**

N.A.

**.18.00.00      EXEMPTIONS TO MONITOR REQUIREMENTS**

N.A.

**.19.00.00      RESERVED**

N.A.

**.20.00.00      PARAMETERS AND CONDITIONS FOR CLOSED LOOP OPERATION**

**General**

The highest conversion efficiency of the catalyst is given in a small window of air-fuel mixture close to the ratio of  $\lambda=1$ . Therefore a combination of two (three for SULEV) control loops is used to achieve the conditions for highest conversion capability of the catalyst. The first control loop uses the signal of the first Oxygen sensor (pre catalyst) to correct the air fuel ratio by adjusting the injection time. The second and third control loop uses the signals of the middle (SULEV) and post catalyst Oxygen sensors. These control loops perform a fine-tuning of the air / fuel ratio to optimise the catalytic conversion.

The first control loop has a quicker response time than the post control loops, which are depending on the death time of the exhaust systems. Therefore the adjustment ranges for the post control loops are restricted and the response time is larger than the one of the first control loop.

**Conditions for closed loop operation of the first control loop**

The main condition for closed loop is a proper heated up Oxygen sensor and the dew point must be exceeded. To guaranty the Oxygen sensor readiness the heat-up strategy starts depending on engine temperature first on a low level of heater power. Upon the exhaust temperature reaches a level where no liquid water is expected to be in the exhaust system the heater power is controlled to achieve normal ceramic temperature of the Oxygen sensor. The ceramic temperature has to be  $>350\text{ }^{\circ}\text{C}$  for binary and  $>685\text{ }^{\circ}\text{C}$  linear sensors. Specific temperatures are mentioned in the individual summary tables of the concepts.

Additional heat-up of the Oxygen sensor is caused by the thermal energy of the exhaust gas. The engine management system evaluates permanently engine temperature and thermal energy introduced to calculate the exhaust temperature based on a model. The main value therefore is the integrated air mass after engine start. Upon the integrated air mass exceeds an applicable threshold, depending on engine start temperature, the dew point is exceeded. In that case, the heater power will be increased until the sensor readiness is achieved and sensor is considered to be ready for closed loop control.

The criteria for sensor readiness of a binary sensor are:

- No fault from heater final stage check
- Sensor signal is out of a range  $0,4\text{V} < \text{sensor voltage} < 0,5\text{V}$
- Heater power  $> 50\%$  within a certain time (typically 8-10 s)

The criteria for sensor readiness of the linear are:

- No fault from LSU-Heater, LSU-Signals and LSU-IC
- LSU is heated up to a ceramic-temperature of  $> 685^{\circ}\text{C}$  or the internal sensor resistor  $R_i < 130\ \Omega$ .

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Parameters evaluated to begin closed loop (first control loop)

The target is to begin closed loop operation in a very early state after engine start. However closed loop is delayed if engine is operated according the catalyst heat-up strategy. In the table below the importance parameters are listed.

Parameter / System	Condition/Evaluation	Monitor
Oxygen Sensor	No fault detected in Oxygen sensor, wiring of the sensor or the sensor IC (linear sensors).	Oxygen sensor monitor for the front sensor(s)
Dew Point exceeded	Exhaust Temperature > threshold, calculated based on mass airflow integral.	Monitor of the mass air flow meter (out of range, rationality)
Oxygen Sensor Readiness	Sensor heated up, evaluated based on heater resistance.	Monitored by diagnostic of the heater control.
Mass Air Flow	Integrated air mass > threshold	Out of range / rationality
Oxygen Sensor Heater	OBD evaluation on sensor heater finished without fault	Oxygen sensor heater monitor.
Engine Load	Calculated value based on mass airflow and fuel injection.	Fuel system monitor, mass air flow meter monitor
Engine Temperature	Signal used to trigger the model calculation.	Monitor for engine coolant temperature sensor (out of range, rationality). Monitor of the cooling system (rationality).
Intake Air Temperature	Signal used to trigger the model calculation.	Monitor for the intake air temperature sensor (out of range)
Secondary Air System	No fault in the secondary air system is detected by OBD.	Monitor for the secondary air system.
Fuel injectors	OBD evaluation on injectors finished without fault	Monitor for the fuel injectors (out of range). Fuel system monitor
Ignition system	OBD evaluation on ignition system finished without fault. No misfire detected.	Monitor for the ignition system (out of range). Misfire monitor.

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Continuity of closed loop operation (first control loop)

The closed loop operation is the most dominant operation mode for the fuel system. Despite that fact, there are operating conditions of the engine where closed loop control must be temporary disabled.

Parameter / System	Condition/Evaluation	Monitor
Target Lambda	Control range is within normal values of Lambda ( $0.8 < \lambda < 1.5$ )	Fuel system monitor, mass air flow meter monitor, oxygen sensor monitor
Engine load	Engine load is too low, to control the exhaust lambda value during SAI (typically relative engine load < 15%)	Fuel system monitor, mass air flow meter monitor, oxygen sensor monitor
Secondary air injection	During the monitor of air injection the target Lambda is commanded to determine deviation cause by air mass.	Fuel system monitor, mass air flow meter monitor
Fuel Injection	Injection time is not at minimum threshold. Injection is not disabled. Fuel cut is not commanded (e.g. coasting)	Monitor for the ignition/injection system (out of range). Misfire monitor. Fuel system monitor

### Typical Values

Given a normal cold started FTP (around 20°C) most of the concepts reaches the closed loop condition for the first control loop within 20s to 60s. Additionally closed loop is forced depending on engine start temperature after a maximum time.

Vehicles produced in MY 2004 and MY 2005

Engine Start Temperature	Time, when closed loop is forced
Temperature $\geq 10$ °C	120 s
Temperature $\geq -6.7$ °C and $< 10$ °C	300 s

**.21.00.00      PARAMETERS / CONDITIONS FOR 2<sup>ND</sup> CLOSED LOOP OPERATION**

**Conditions for closed loop operation of the second control loop**

As already mentioned under "General" the 2<sup>nd</sup> control loop optimises the adjustments of the first control loop over a longer time to achieve the maximum conversion of the catalyst in a very small window of air/fuel ratio close to  $\lambda=1$ . The second control loop uses a binary Oxygen sensor, which is operated at a target value of sensor output voltage. Deviations from the target voltage are corrected by adjusting the air/fuel ratio until the target voltage is achieved again. The controller of the 2<sup>nd</sup> control loop is a combination of proportional and integral (PI-) controller. The proportional and the integral portion of the controller have individual enable criteria.

**Parameters evaluated to begin closed loop (second control loop)**

**Enable criteria for P-portion of the controller**

The proportional-portion of the controller corrects short-term deviations and achieves the target sensor output voltage.

<b>Parameter / System</b>	<b>Condition/Evaluation</b>	<b>Monitor</b>
Closed loop condition for the <b>first control loop</b> . Minimum of integrated mass airflow passed.	No fault detected in wiring of the sensor or the sensor IC (linear sensors). Fuel control performs normal, no fault is detected and fuel control is not temporarily disabled.	Oxygen sensor monitor for the front sensor(s). Monitor of the mass air flow meter (out of range, rationality). Fuel system monitor
Oxygen Sensor for 2 <sup>nd</sup> control loop readiness	Sensor heated up, a minimum power was delivered to the heater, sensor voltage has left the voltage range of a cold sensor	Monitored by diagnostic of the heater monitor and sensor-wiring monitor.
Catalyst model temperature	Exhaust Temperature > threshold, calculated based on mass airflow integral, ignition timing, lambda value, vehicle speed.	Monitor of the mass air flow meter (out of range, rationality) Fuel system monitor, oxygen sensor monitor, vehicle speed sensor monitor
Variable Valve Timing System (if applicable)	No fault detected	VVT monitor
Secondary Air System	No fault detected	AIR System monitor
EVAP purge System	No fault detected	EVAP purge monitor
Mass Air Flow Meter	No fault detected	Mass Air Flow Meter monitor
Controller range for the first control loop is not at the threshold limit.	Controller for the first control loop not at minimum or maximum threshold	Oxygen sensor monitor

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Enable criteria for adaptive I-portion of the controller (additionally)

The integral-portion of the controller corrects permanent deviations / shifts over a longer time by adjusting the adaptation.

Parameter / System	Condition/Evaluation	Monitor
Engine speed/load within a normal operating range	Engine Speed within 1500-4000 rpm Engine Load within 20-60%  (Typical values; may differ on individual concepts)	Engine Speed Sensor monitor, Mass Air Flow Meter monitor, and fuel system monitor.
Carbon Canister of the EVAP system	High load of carbon canister indicated during EVAP purge.	EVAP purge monitor.
Minimum of integrated mass airflow passed and P-portion of controller achieves target range for Oxygen sensor voltage already.	Oxygen sensor voltage of 2 <sup>nd</sup> control loop, P-portion of controller for 2 <sup>nd</sup> control loop	Oxygen sensor monitor for secondary sensor(s). Fuel system monitor

### Typical Values (second control loop)

Given a normal cold started FTP (around 20°C) most of the concepts reaches the closed loop condition for the second control loop within 60s to 100s.

**.22.00.00      PARAMETERS / CONDITIONS FOR CLOSED LOOP OPERATION ON SULEV**

**General**

The SULEV concept consists of 2 catalysts and 3 control loops. The first control loop uses the Oxygen sensor pre catalyst (LSU) in the same manner conventional concepts does. The Oxygen sensor between the two bricks (LSF1) of the catalyst is the input for the second and the Oxygen sensor after the last brick (LSF2) is the input for the third control loop. Both sensors are binary Oxygen sensors. The closed loop operation of each of the control loops are in a depending order of 1<sup>st</sup>, 2<sup>nd</sup> and 3<sup>rd</sup> control loop. In comparison to post catalyst control loop on conventional concepts the 2<sup>nd</sup> and 3<sup>rd</sup> control loop are high precision loops with specific requirements for short-term correction and long-term adaptation. The driving conditions have to be stable and constant to allow any corrections by these control loops. The allowed correction steps are much smaller in comparison to post catalyst control loop applications on conventional concepts.

**Conditions for closed loop operation of the first control loop**

The conditions for closed loop operation of the first control loop on the SULEV concept are the same as described for conventional concepts.

**Conditions for closed loop operation of the second control loop**

The second control loop on the SULEV concept is designed as natural frequency control loop and is based on a binary Oxygen sensor. The controller has the same capability in achieving maximum conversion on the first brick of the catalyst by using a proportional adjustment range for short-term correction and an integral adjustment range for long-term adaptation (PI-controller). Both controller ranges have individual conditions for closed loop operation.

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Enable criteria for P-portion of the controller of second control loop (SULEV)

The proportional-portion of the controller corrects short-term deviations.

Parameter / System	Condition/Evaluation	Monitor
Closed loop condition for the <b>first control loop</b> . Minimum of integrated mass airflow passed.	No fault detected in wiring of the sensor or the sensor IC (linear sensors). Fuel control performs normal, no fault is detected and fuel control is not temporarily disabled.	Oxygen sensor monitor for the front sensor(s). Monitor of the mass air flow meter (out of range, rationality). Fuel system monitor
Oxygen Sensor for 2 <sup>nd</sup> control loop readiness	Sensor heated up, a minimum power was delivered to the heater, sensor voltage has left the voltage range of a cold sensor	Monitored by diagnostic of the heater monitor and sensor-wiring monitor.
Engine Coolant Temperature	Engine coolant temperature has raised above a limit value of 50 °C (Typical temperature value; may differ on specific application)	Engine Coolant Temperature Sensor Monitor. Engine Cooling System Monitor.
Catalyst model temperature	Exhaust Temperature > threshold (above light-off temperature), calculated based on mass airflow integral, ignition timing, lambda value, vehicle speed.	Monitor of the mass air flow meter (out of range, rationality) Fuel system monitor, oxygen sensor monitor, vehicle speed sensor monitor
Variable Valve Timing System (if applicable)	No fault detected	VVT monitor
Secondary Air System	No fault detected	AIR System monitor
EVAP purge System	No fault detected	EVAP purge monitor
Mass Air Flow Meter	No fault detected	Mass Air Flow Meter monitor
Controller range for the first control loop	Controller for the first control loop not at minimum or maximum threshold	Oxygen sensor monitor

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Enable criteria for adaptive I-portion of the controller second control loop (additionally)

The integral-portion of the controller corrects permanent deviations / shifts over a longer time by adjusting the adaptation.

Parameter / System	Condition/Evaluation	Monitor
Engine speed/load within a normal operating range	Engine Speed within 1500-5000 rpm Engine Load within 15-100%  (Typical values; may differ on individual concepts)	Engine Speed Sensor monitor, Mass Air Flow Meter monitor, and fuel system monitor.
Carbon Canister of the EVAP system	High load of carbon canister indicated during EVAP purge.	EVAP purge monitor.
Minimum of integrated mass airflow passed and P-portion of controller achieves target range for Oxygen sensor voltage already.	Oxygen sensor voltage of 2 <sup>nd</sup> control loop, P-portion of controller for 2 <sup>nd</sup> control loop	Oxygen sensor monitor for secondary sensor(s). Fuel system monitor

### Typical Values (second control loop)

Given a normal cold started FTP (around 20°C) most of the concepts reaches the closed loop condition for the second control loop within 60s to 80s.

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Conditions for closed loop operation of the third control loop

The third control loop is designed like the second control loop on conventional concepts and achieves the maximum conversion of the 2<sup>nd</sup> brick of the catalyst. The controller consists of very restricted correction ranges for the short-term proportional and the long-term integral adaptive portion (PI-controller). Both controller ranges have individual conditions for closed loop operation.

### Enable criteria for P-portion of the controller of third control loop (SULEV)

The proportional-portion of the controller corrects short-term deviations.

Parameter / System	Condition/Evaluation	Monitor
Closed loop condition for the <b>first control loop</b> . Minimum of integrated mass airflow passed.	No fault detected in wiring of the sensor or the sensor IC (linear sensors). Fuel control performs normal, no fault is detected and fuel control is not temporarily disabled.	Oxygen sensor monitor for the front sensor(s). Monitor of the mass air flow meter (out of range, rationality). Fuel system monitor
Closed loop condition for the <b>second control loop</b> . Minimum of integrated mass airflow passed.	No fault detected in LSU System (Sensor, wiring, IC) and no fault at LSF1 and LSF2. Fuel control performs normal, no fault is detected and fuel control is not temporarily disabled.	Oxygen sensor monitor for the front sensor(s). Oxygen sensor monitor for the first downstream sensor(s) and Oxygen sensor monitor for the second downstream sensor(s). Monitor of the mass air flow meter (out of range, rationality). Fuel system monitor
Oxygen Sensor for 3 <sup>rd</sup> control loop readiness	Sensor heated up, a minimum power was delivered to the heater, sensor voltage has left the voltage range of a cold sensor	Monitored by diagnostic of the heater monitor and sensor-wiring monitor.
Catalyst model temperature	Exhaust Temperature > threshold (above light-off temperature), calculated based on mass airflow integral, ignition timing, lambda value, vehicle speed.	Monitor of the mass air flow meter (out of range, rationality) Fuel system monitor, oxygen sensor monitor, vehicle speed sensor monitor
Variable Valve Timing System (if applicable)	No fault detected	VVT monitor
Secondary Air System	No fault detected	AIR System monitor
EVAP purge System	No fault detected	EVAP purge monitor
Mass Air Flow Meter	No fault detected	Mass Air Flow Meter monitor
Controller range for the first control loop	Controller for the first control loop not at minimum or maximum threshold	Oxygen sensor monitor

(LSU: Linear Oxygen Sensor, LSF1: 1<sup>st</sup> Binary Oxygen Sensor, LSF2: 2<sup>nd</sup> Binary Oxygen Sensor)

## Bosch Motronic ME 7, ME 7.1, ME 7.1.1, ME 7.5 System Strategy

### Enable criteria for adaptive I-portion of the controller third control loop (additionally)

The integral-portion of the controller corrects permanent deviations / shifts over a longer time by adjusting the adaptation.

Parameter / System	Condition/Evaluation	Monitor
Engine speed/load within a normal operating range	Engine Speed within 2700-3500 rpm Engine Load within 25-45%  (Typical values; may differ on individual concepts)	Engine Speed Sensor monitor, Mass Air Flow Meter monitor, and fuel system monitor.
Carbon Canister of the EVAP system	High load of carbon canister indicated during EVAP purge.	EVAP purge monitor.
Minimum of integrated mass airflow passed and P-portion of controller achieves target range for Oxygen sensor voltage already.	Oxygen sensor voltage of 2 <sup>nd</sup> control loop, P-portion of controller for 2 <sup>nd</sup> control loop	Oxygen sensor monitor for secondary sensor(s). Fuel system monitor

### Typical Values (third control loop)

Given a normal cold started FTP (around 20°C) most of the concepts reaches the closed loop condition for the third control loop within 90s to 100s.